Modeling of liquid nuclear waste vitrification: focus on the chemical processes

Z. Nabyl ^{*1}, S. Schuller ², R. Podor ³, J. Lautru ³, G. Quintard ³, C. Castano ¹, A. Artico ¹, V. Benavent¹, M. Delaunay¹, E. Sauvage¹

¹ CEA/DES/ISEC/DPME/LDPV, Université de Montpellier, Marcoule, France ² CEA/DES/ISEC/DPME, Université de Montpellier, Marcoule, France ³ ICSM, UMR 5257 CEA-CNRS-UM2-ENSCM-F-20207 Bagnols sur Cèze, France

CONTEXT AND OBJECTIVES

- High-level nuclear waste: processing in **glass**, stable and sustainable at the atomic scale
 - Vitrification process in France: . Nitric solution of nuclear fission and actinide product
 - **Calcination** of nitric solution with calcination additive
 - Addition of calcine and glass frit in the vitrification melter
- **3D multi-physics modeling of high-level nuclear waste vitrification process** in cold crucible [1,2]
- Chemical and thermal reactions during calcine dissolution in the glass [3,4]
- Other way of vitrification, by **liquid feeding:** liquid radioactive waste directly added at the surface of vitrification melter -> No modeling of liquid feeding vitrification process yet



<u>* zineb.nabyl@cea.fr</u>





Modeling of vitrification process in cold crucible. Coupling of the 0D thermal kinetic model to the 3D model [3].

Vitrification of simulated nuclear waste at experimental scale, with a mechanical agitator

 \rightarrow Acquire the chemical data needed to model liquid radioactive waste vitrification process \rightarrow Predict and optimise vitrification process by liquid feeding







Crushing





Thermal treatment

GLASS CHARACTERISATION

- Evolution of glass morphology and secondary compound formation and dissolution in function of temperature and time
- Order of dissolution in the glass: Ca-REE silicate, Ce- oxide, Zr- (Ce-) oxide



METHODOLOGY

- Characterize the **secondary phases** and the **chemical reaction** between the liquid solution and glass frit
- Determine the **chemical kinetic** of the liquid dissolution in the glass frit

Noyes-Witney equation (1897) $C_i(t) = C_{is}(1 - e^{\overline{\tau_i}})$

- Experiments of thermal treatment, in muffle furnace at 800 to **1200°C** and during **2-5-30-120-480 minutes** (25 samples)
- Study of glass microstructure and phase identification
- Analytical protocol to study glass composition and element concentration evolution (SEM)
 - → Parameterization of concentration evolution; kinetic parameters relative to waste liquid dissolution in glass frit



Glass

900°C – 30 min

SEM chemical mapping (Ca, La, Ce, Nd, Pr and Zr) from the sample synthesised at 900°C and during 30 minutes.

1200°C



BSE images of the glass morphology and secondary phase evolution in time at 800 and 1200°C.

DISSOLUTION KINETIC



- C_s (saturation concentration) and τ (saturation time) for Zr, Ce and Nd), at each temperature
- **Ea** (activation energy) and **A** (pre-exponential factor)
- Secondary phase formation: Zr- (Ce-) oxide and Ce- oxide -> inherited from the dried solution, dissolution in the glass frit

- Ca-REE- silicate -> intermediate compounds, formation from the dried solution dissolution





Temperature (°C) 1200 1100 Phases: **Ca-REE- silicate** Ce- oxide 1000 Zr- (Ce-) oxide 900 800

References: [1]. Sauvage E., PhD thesis (2007); [2] Barba Rossa G., PhD thesis (2017); [3] Paraiso K., PhD thesis (2021); [4] Paraiso et al., Journal of Nuclear Materials, 569, 153878 (2022)