

# Molecular dynamics simulations of nuclear waste glasses and their aqueous corrosion behaviors

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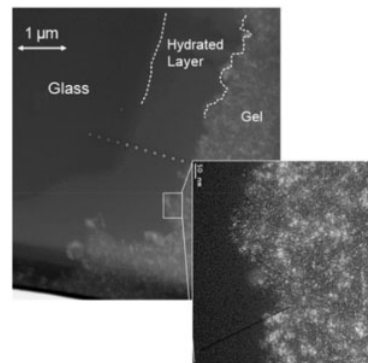
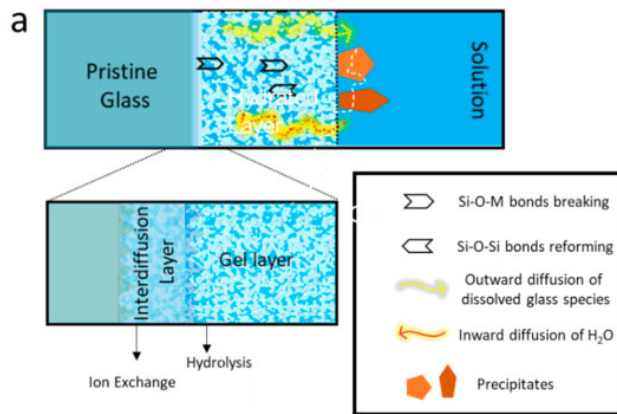
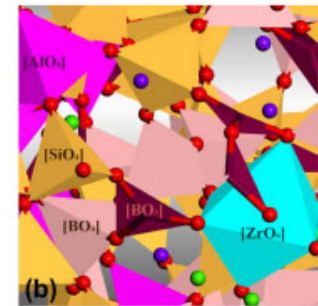
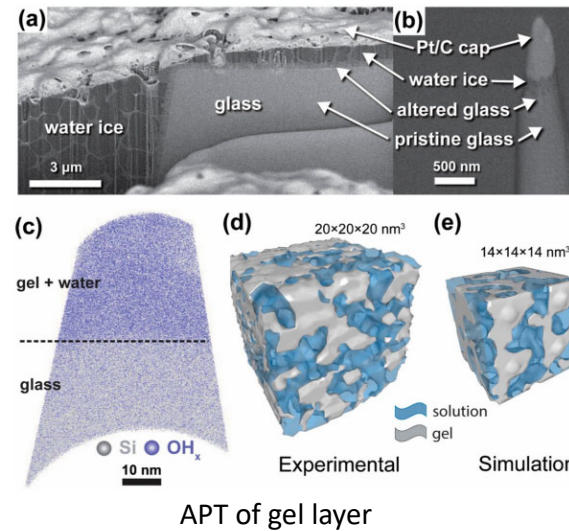


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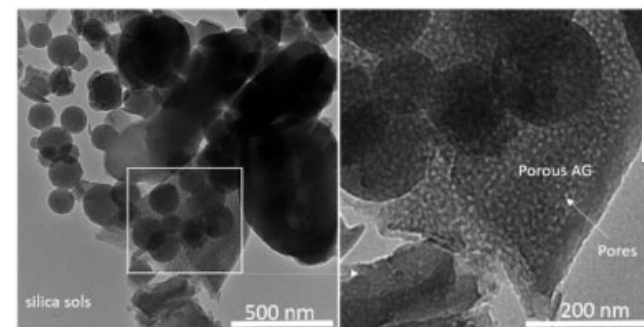


# Advances in understanding glass corrosion

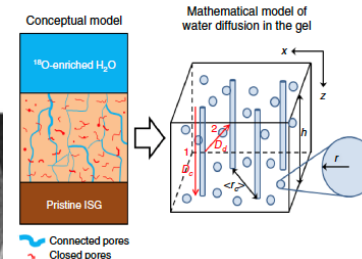
- Glass corrosion is a complex process with coupled interfacial reactions and ion transport behaviors.
- For nuclear waste glasses, the complexity of composition and glass structure further complicated the problem.
- Various experimental techniques have been used to study glass corrosion: NMR, SIMS, XPS, SEM/TEM, APT, SHG.
- Simulations have also been applied to investigate glass corrosion: MD, MC, AIMD, machine learning approaches.



SEM image of interface



TEM image of gel layer



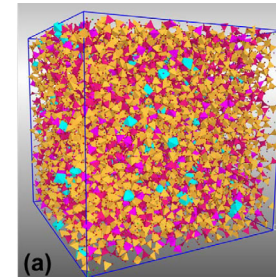
Gin et al. Nature Comm. 9(2018)2169

Frankel et al. Chem. Rev. 121(2021)12327

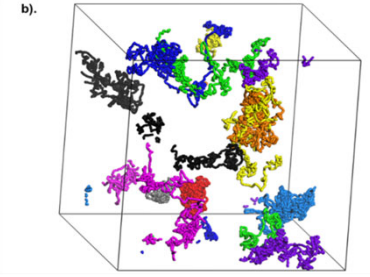
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# What can MD simulations contribute to understand glass corrosion?

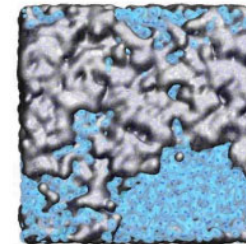
- Obtain accurate atomic structural models of multicomponent nuclear waste glasses
- Calculate diffusion rate and energy barriers: cations, anions and water molecules
- Determine energy barriers for particular reactions (ion exchange, hydrolysis etc.)
- Identifying reaction mechanisms: ion exchange, hydrolysis, water transport etc.
- Gel layer formation and water/ion transport
- Glass surface morphology evolutions
- ML and MD based QSPR analysis of corrosion rate
- Monte Carlo simulations with glass structure model from MD simulations



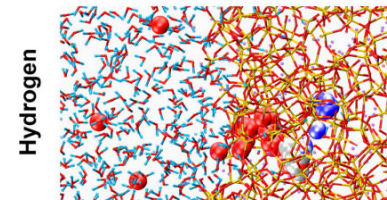
(a) Gin et al. Nature Comm. 2018



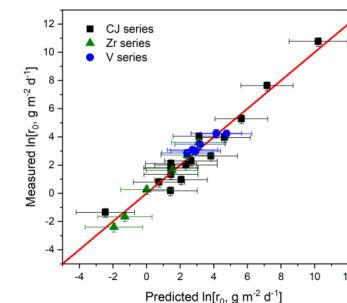
b). Rimsza, Du, JPCC 2017



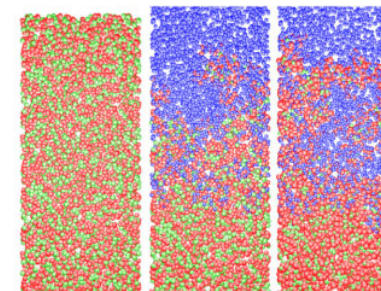
Mahadevan, Du, JNCS 2023



Deng et al. npj Mater Degr. 2019



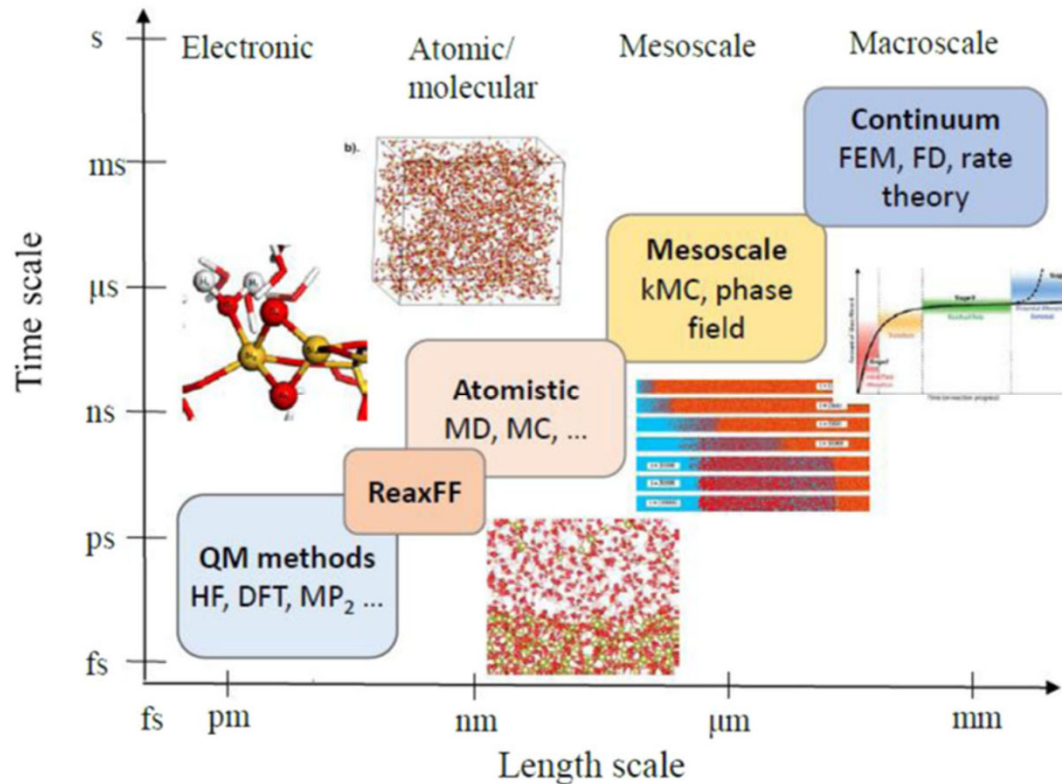
Lu et al. JACerS 106(2022)1025



Kerisit, Du JNCS 522(2019)119601

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# Computer simulation methods



**Quantum Mechanical method:**

$$\left[ \frac{-\hbar^2}{2m} \nabla^2 + V \right] \Psi = i \hbar \frac{\partial}{\partial t} \Psi$$

**Molecular Dynamic method:**

$$\mathbf{f}_i = m_i \ddot{\mathbf{r}}_i = m_i \frac{\partial^2 \mathbf{r}_i}{\partial t^2}$$

**Monte Carlo method:**

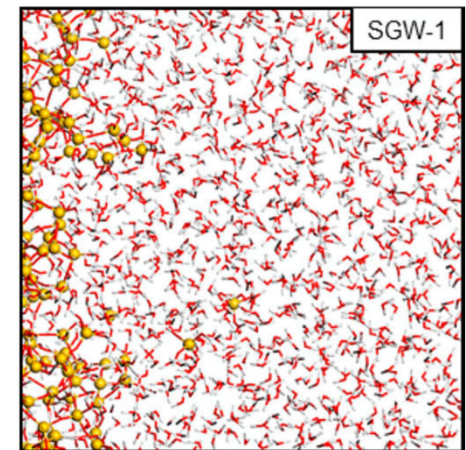
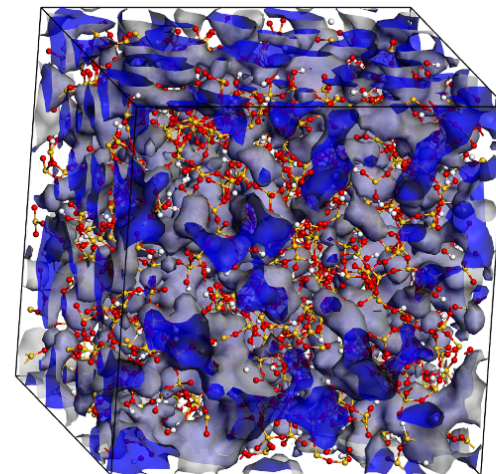
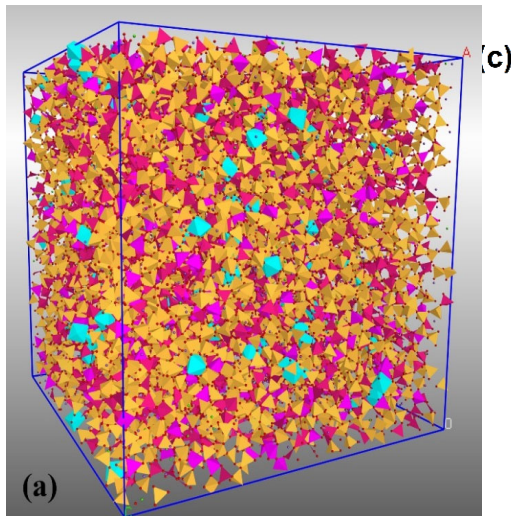
$$p = \exp(-\Delta E/kT)$$

**Rate theory:**

$$r_2 = k_+(H^+)^n e^{-\frac{E_a}{RT}} \left( 1 - \frac{Q}{K} \right)$$

*Du and Rimsza, NPJ Mater. Degrad. 1(2017)6*

# Fundamental Understanding of Glass Corrosion from atomistic simulations



Glass structure models



Gel structure and  
water diffusion



Interfacial structure  
and evolution

## Multicomponent glass dissolution mechanism & rate predictions

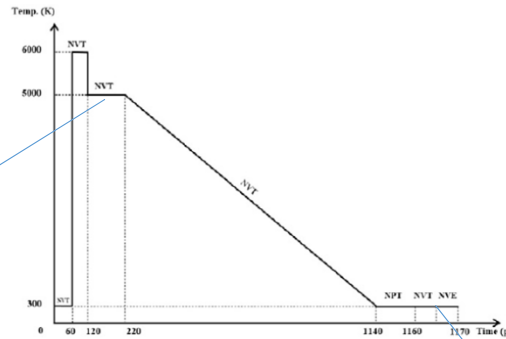
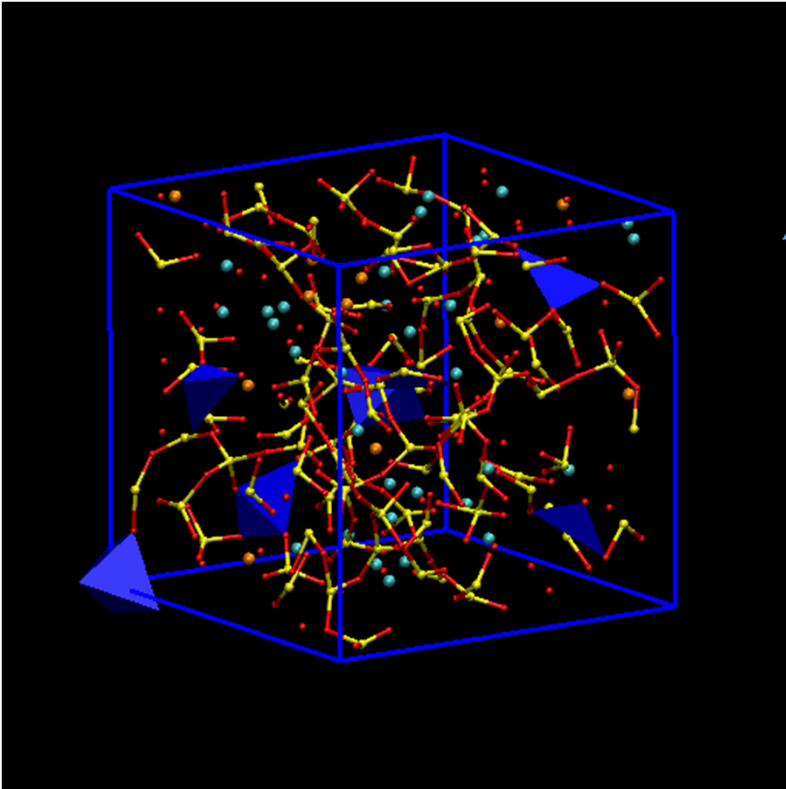
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# MD simulation of glass formation

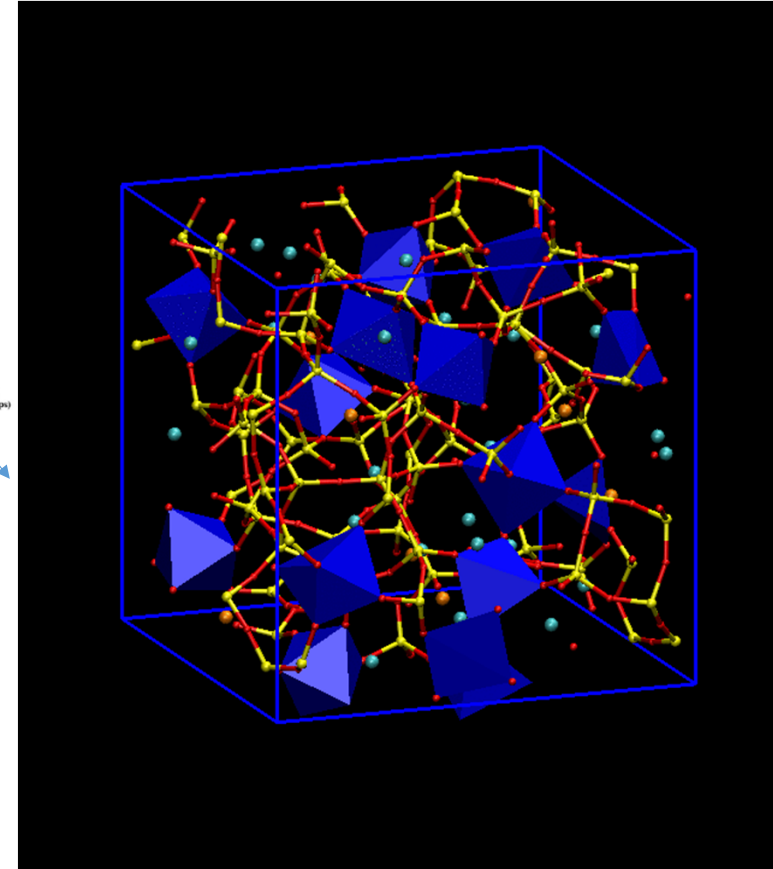
Melt at 5000 K

Glass at 300 K



Red: O  
Yellow: Si  
Green: Na  
Pink: Ca  
Blue polyhedral: [ZrO<sub>6</sub>]

MD simulation of a ZrO<sub>2</sub> containing soda lime silicate glass. (Lu et al., JNCS 2018)



# Potential development for multicomponent borosilicate glasses

$$V(r_{ij}) = \frac{Z_i Z_j e^2}{4\pi\epsilon_0 r_{ij}} + A_{ij} \exp(-r_{ij}/\rho_{ij}) - C_{ij}/r_{ij}^6$$

$$V'(r_{ij}) = B_{ij}/r_{ij}^n + D_{ij} \cdot r_{ij}^2$$

Du and Cormack, *J. Am. Ceram. Soc.* 88(2005)2532

Du and Corrales, *JNCS* 352(2006)3255

Du et al., *J. Am. Ceram. Soc.* 94(2011)2393

$$A_{B-O} = \begin{cases} A_1 + t_1 \times (R_{max} - (R_{max} - N_4)^2 / R_{max}) + t_2 \times K^2 & R \leq R_{max} \\ A_2 + t_3 \times R_{max} \times N_4 / R & R \geq R_{max} \end{cases}$$

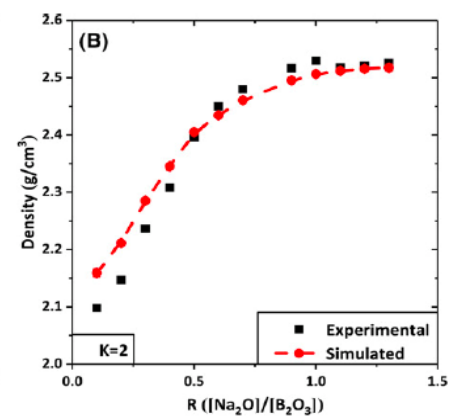
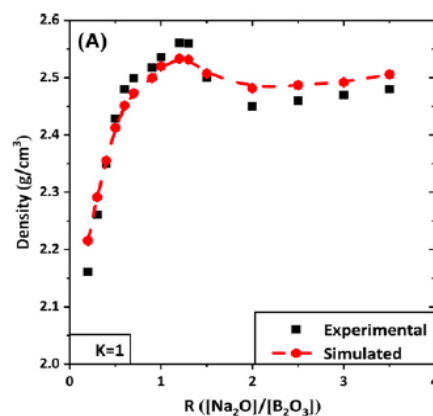
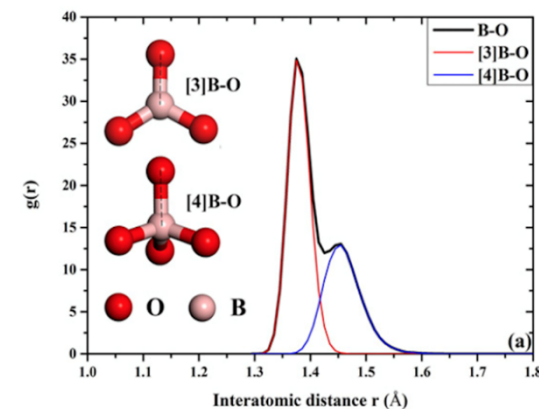
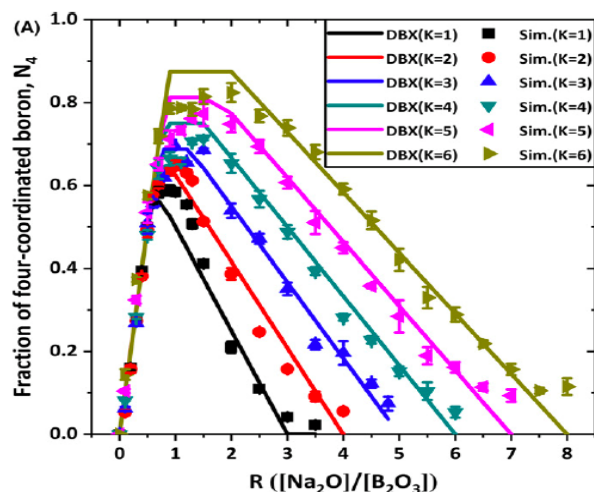
$$t_3 = (A_1 + t_2 \times K^2 - A_2 / R_{max} + t_1)$$

Variable	A <sub>1</sub> (eV)	A <sub>2</sub> (eV)	t <sub>1</sub> (eV)	t <sub>2</sub> (eV)
Parameter	11900.00	12525.00	4350.00	85.00

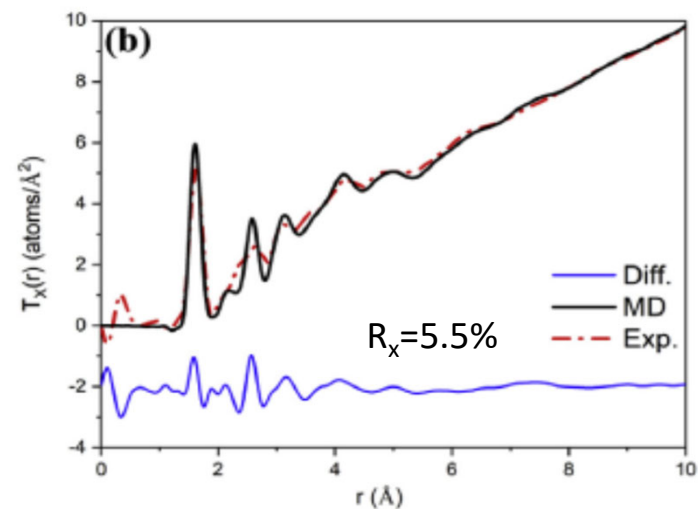
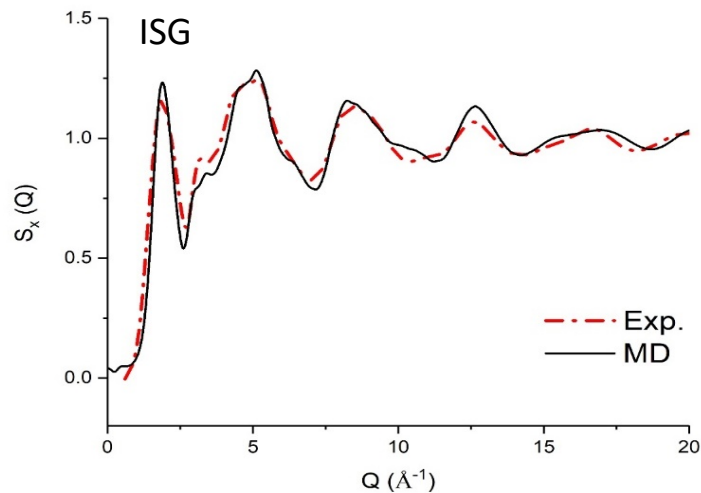
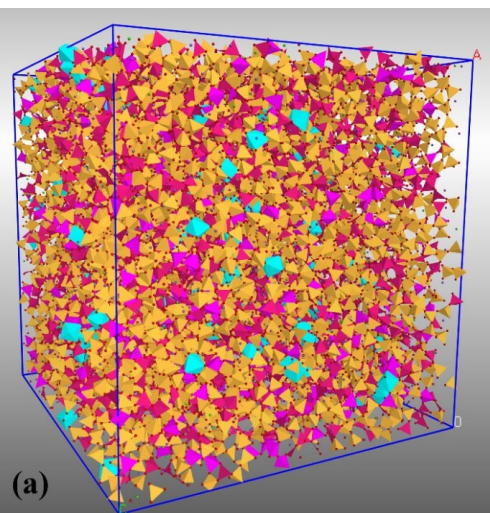
Lu et al. *J. Phys. Chem. B.* 122(2018)2564

Lu, Deng, Sebastien, Du, *NPJ Mater. Degrad.* 2(2018)19

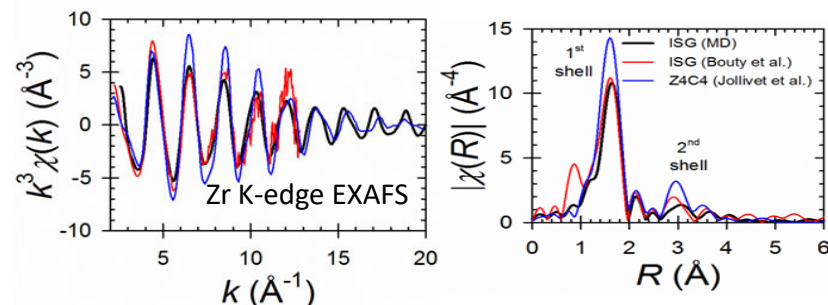
Deng and Du, *J. Am. Ceram. Soc.* 102(2019)2482



# ISG Structures from MD: experimental validations



(mol%)	SiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	B <sub>2</sub> O <sub>3</sub>	CaO	Na <sub>2</sub> O	ZrO <sub>2</sub>
ISG*	60.2	3.8	16.0	5.7	12.6	1.7

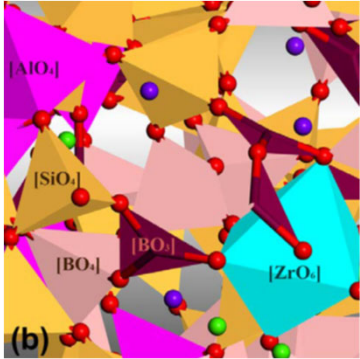


\* Gin et al. *Materials Today*, 16(2013)243

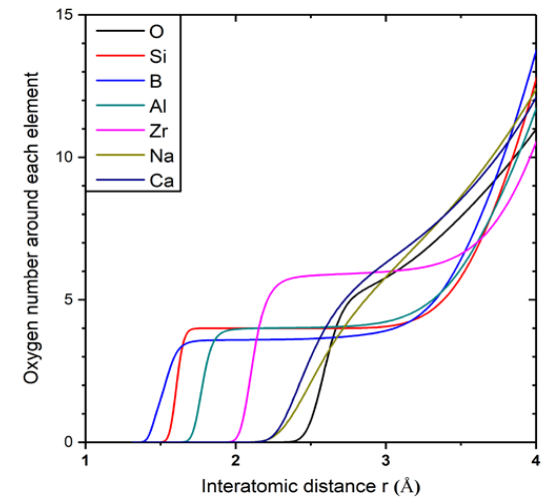
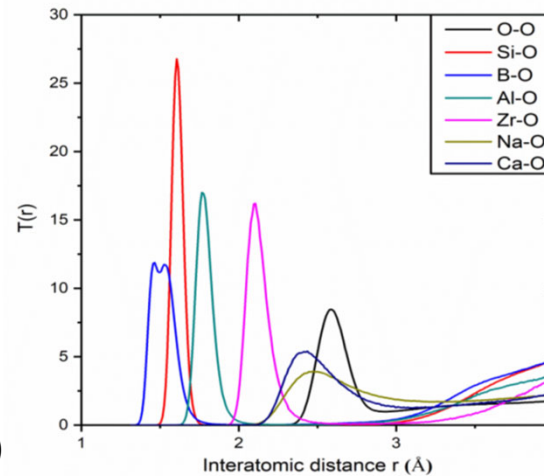
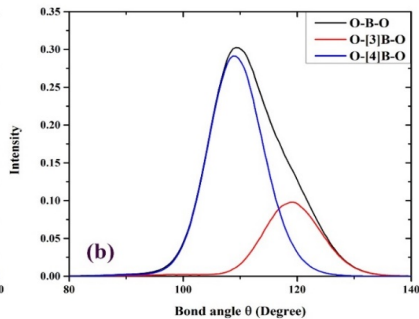
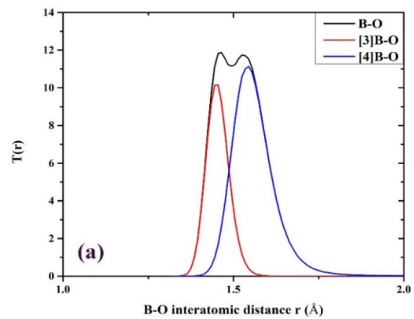
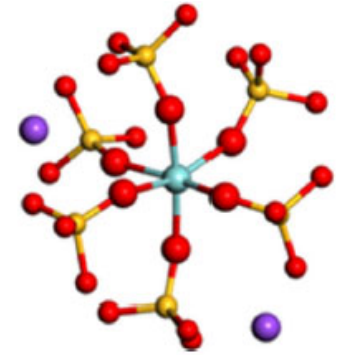
M. Collin et al., *npj Materials Degradation*, 2018;2:4.  
 X. Lu, L. Deng, S. Kerisit, J. Du, *npj Materials Degradation*, 2018; 2:19  
 X. Lu, L. Deng, C. Benmore, J. Du, *J. Nuclear Mater.* 515(2019)284



# ISG glass general structure features



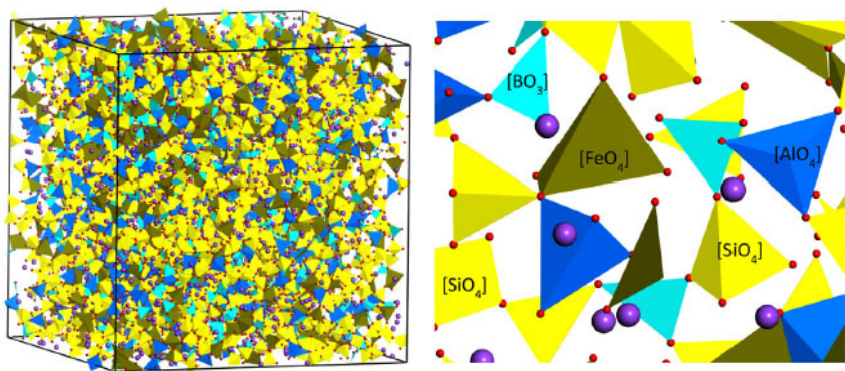
X	$r_{X-O}$ (Å)	$r_{cut}$ (Å)	$CN_{avg.}$	Coordination Number (CN) (%)				
				3	4	5	6	7
Si	1.61	2.25	<b>4.00</b>	--	100	--	--	--
B	1.45 ( <sup>3</sup> B)	2.00	<b>3.59</b>	41.3	58.7	--	--	--
	1.55 ( <sup>4</sup> B)							
Al	1.77	2.25	<b>4.00</b>	0.5	98.6	0.9	--	--
Zr	2.10	2.85	<b>5.68</b>	--	--	10.7	85.7	3.6



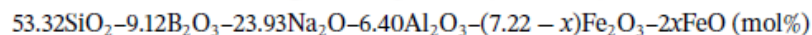
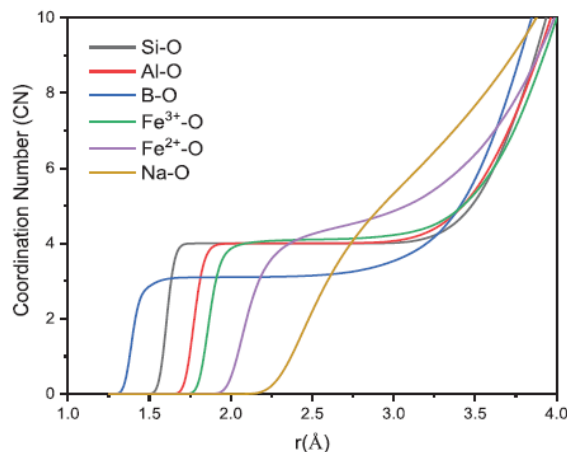
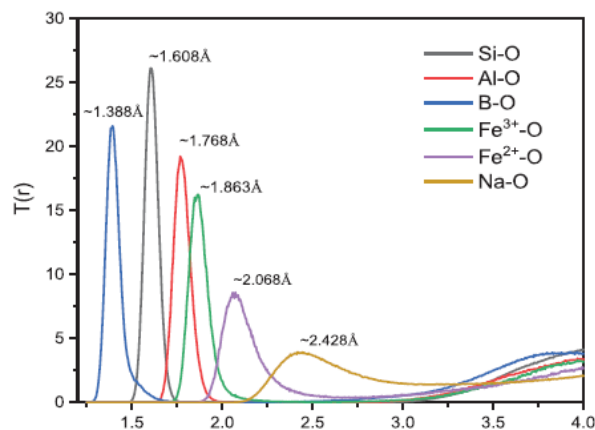
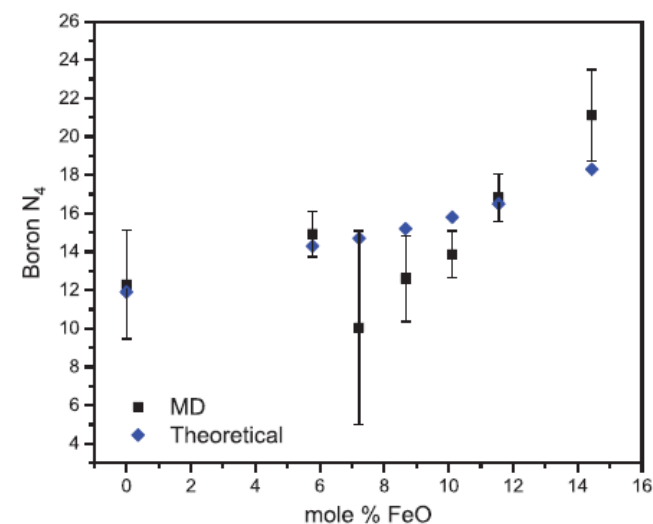
Collin et al. NPJ Mater. Degrad. 2(2018)

SumGlass 2023, Nimes France, du@unt.edu

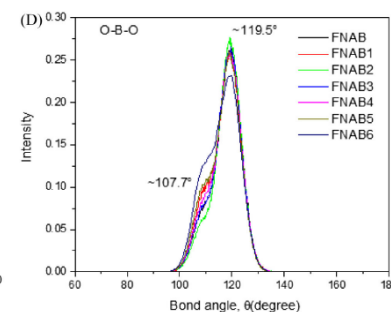
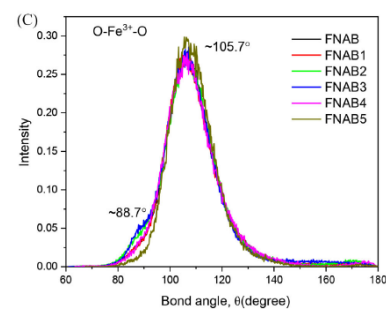
# MD simulations of iron redox ratio effect



- Iron redox ratio effect on the structure of sodium silicate & borosilicate glasses
- $Fe^{3+}$  plays the role of former while  $Fe^{2+}$  plays the role of modifier
- Reduction of iron, lead to an increase of boron  $N_4$  values



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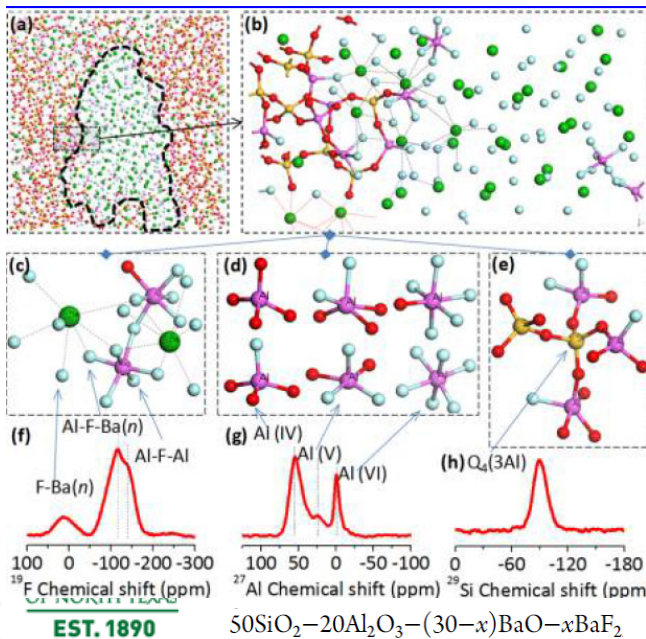
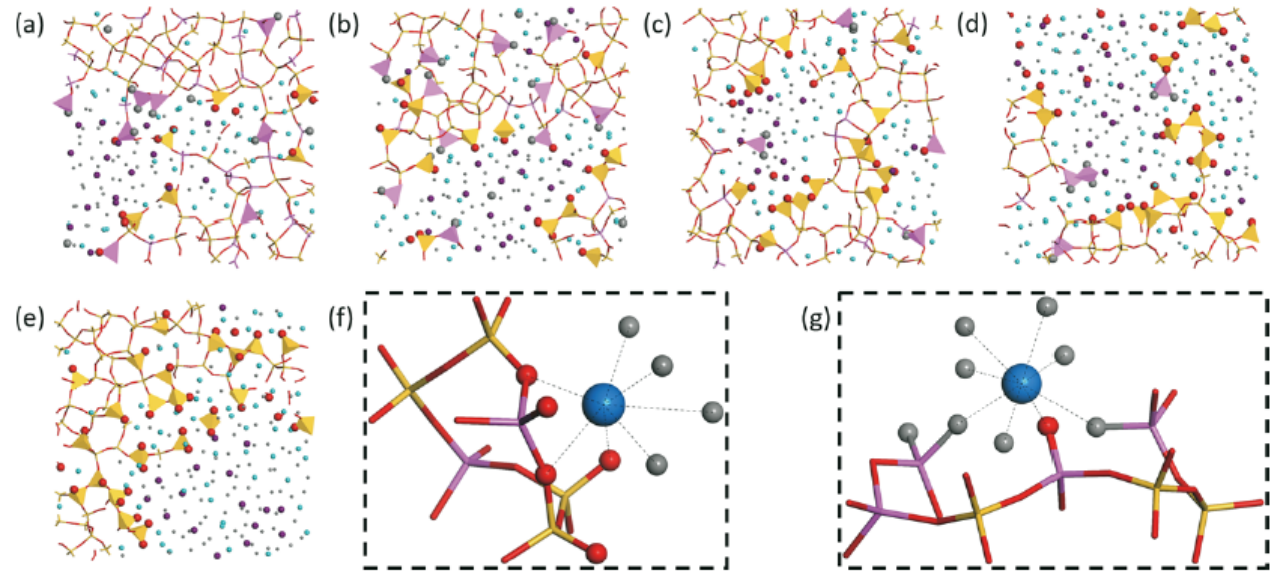
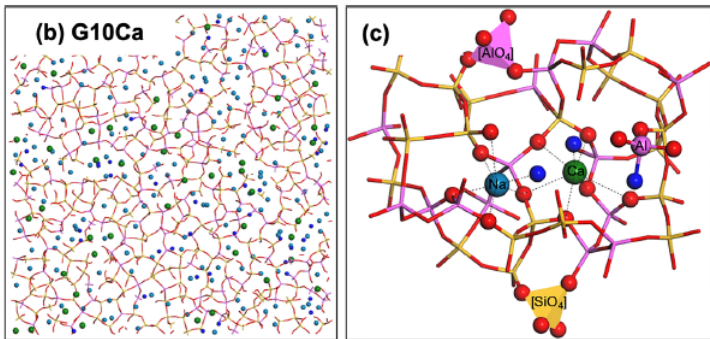
Tuheen, Sun, Du, JACerS, 2022

Nienhuis, Tuheen, Du, McCloy, J Mater Sci. 2021

Balasubramanya, Tuheen, ..., Du, Goel, in prep.



# Phase separation in glasses from MD simulations



- MD simulations of fluorosilicate glasses with CaO/Na<sub>2</sub>O substitution lead to more Ca-F bonds that helps of F retention in waste glasses
- Barium aluminosilicate oxyfluoride glass show phase separation in certain fluoride concentration
- La<sup>3+</sup> were studied in oxyfluoride glasses and found to preferentially exist in the fluoride region

Zhao, Nienhuis, McCloy, Du, JNCS 2020  
 Zhao et al, J Phys Chem. B 2016  
 Zhao et al., J. Phys Chem B, 2020

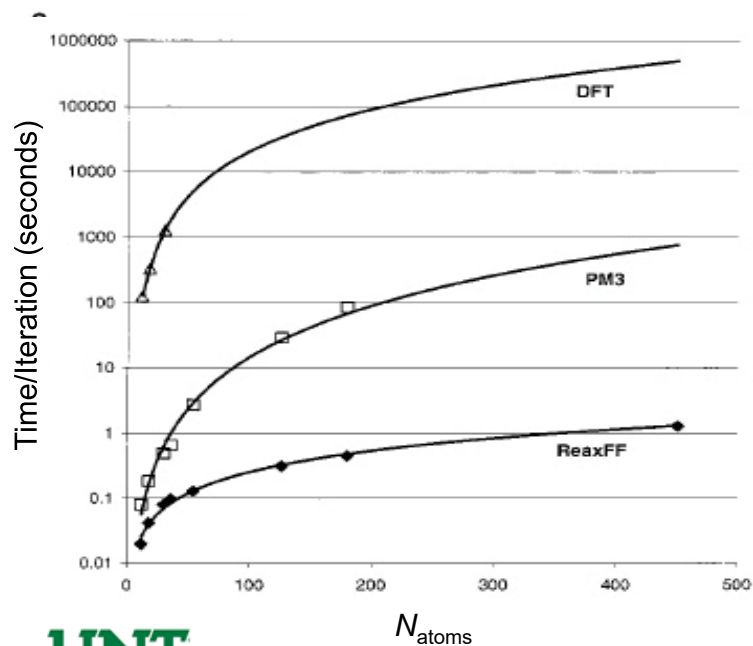
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# Potentials can handle reactions: Reactive Force Field

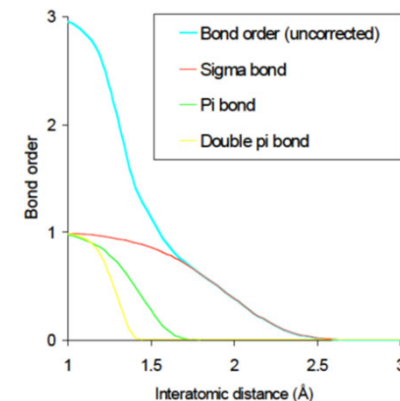
$$E_{\text{potential}} = (E_{\text{bond}} + E_{\text{over}} + E_{\text{under}}) + (E_{\text{valency angle}} + E_{\text{penalty}}) + E_{\text{torsion}}$$

$$+ E_{\text{lone pair}} + E_{\text{conjugation}} + E_{\text{H-bond}} + E_{\text{vdWaals}} + E_{\text{Coulomb}}$$



## Bond order calculations:

$$BO_{ij} = \exp \left[ p_{bo,1} \cdot \left( \frac{r_{ij}}{r_o} \right)^{p_{bo,2}} \right] + \exp \left[ p_{bo,3} \cdot \left( \frac{r_{ij}}{r_o} \right)^{p_{bo,4}} \right] + \exp \left[ p_{bo,5} \cdot \left( \frac{r_{ij}}{r_o} \right)^{p_{bo,6}} \right]$$



$$E_{\text{bond}} = -D_e \cdot BO_{ij} \cdot \exp \left[ p_{be,1} \left( 1 - BO_{ij}^{p_{be,1}} \right) \right]$$

## Charge calculations: Electronegativity Equalization

Method (EEM: Mortier, et al, JACS, 108, 4315, ('86).) to calculate the charge equilibration

$$E = \sum_{i < j} \frac{q_i q_j}{r_{ij}} + \sum_i \left( \chi_i q_i + \frac{1}{2} J_i q_i^2 \right)$$

$$E_{\text{Coulomb}} = C \cdot \frac{q_i \cdot q_j}{\left[ r_{ij}^3 + (1/\gamma_{ij})^3 \right]^{1/3}}$$

# Diffuse Charge Reactive Potential (DCRP)

## 2-body interactions

$$E_{2\text{body}} = E_{\text{qq}} + E_{q^+q^+} + E_{q^+q^-} + E_{q^-q^-} + E_{\text{rep}} + E_{\text{disp}}$$

where

$$E_{\text{qq}} = \frac{q_i q_j}{r_{ij}} \operatorname{erfc}\left(\frac{r_{ij}}{\beta}\right)$$

$$E_{q^+q^+} = E_{q^+q^-} = \frac{q_i q_j}{4r_{ij}} \operatorname{erf}\left(\frac{r_{ij}}{\sqrt{2}\xi_{ij}}\right) \operatorname{erfc}\left(\frac{r_{ij}}{\beta}\right)$$

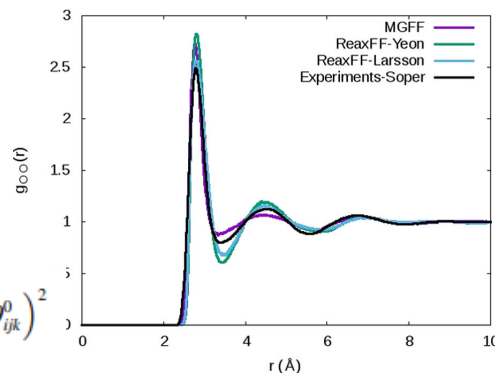
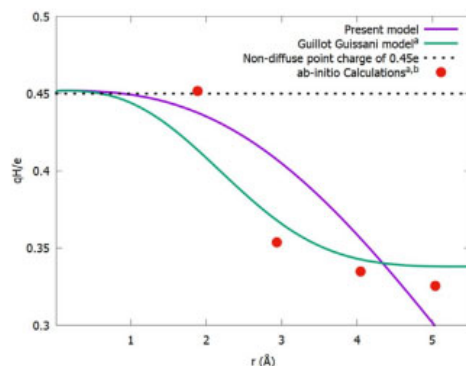
$$E_{q^-q^-} = \frac{q_i q_j}{16r_{ij}} \operatorname{erfc}\left(\frac{r_{ij}}{2\xi_{ij}}\right) \operatorname{erfc}\left(\frac{r_{ij}}{\beta}\right)$$

$$E_{\text{rep}} = A_{\text{rep}}^{ij} \frac{\operatorname{erfc}(z_{ij})}{z_{ij}} \quad \left[ \text{with } z_{ij} = \frac{r_{ij}}{2\xi_{ij}} \right]$$

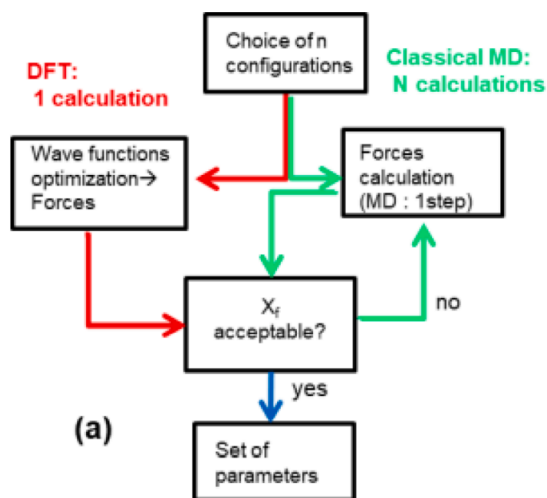
$$E_{\text{disp}} = \frac{-C_6^{ij}}{r_{ij}^6}$$

## 3-body interactions

$$U_{ijk}^{\text{thr}} = \lambda_{ijk} \exp\left(\frac{\gamma_{ij}}{r_{ij} - r_{ij}^0} + \frac{\gamma_{ik}}{r_{ik} - r_{ik}^0}\right) (\cos\theta_{ijk} - \cos\theta_{ijk}^0)^2$$

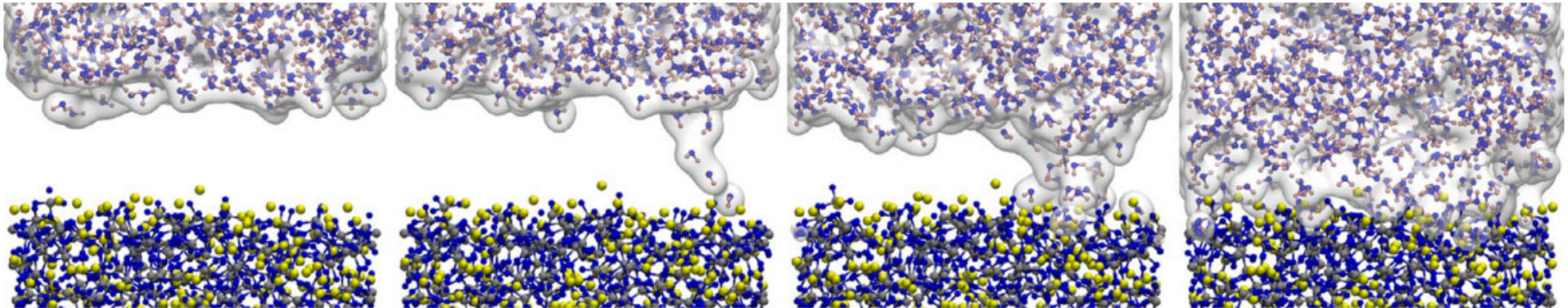


Mahadevan, Garofalini, J. Phys. Chem. C 112(2008)1507  
 Mahadevan, Wei, Du, J. Am. Ceram. Soc. 103(2020)3676  
 Mahadevan et al. J. Non-Cryst. Solids, 592(2022)121764

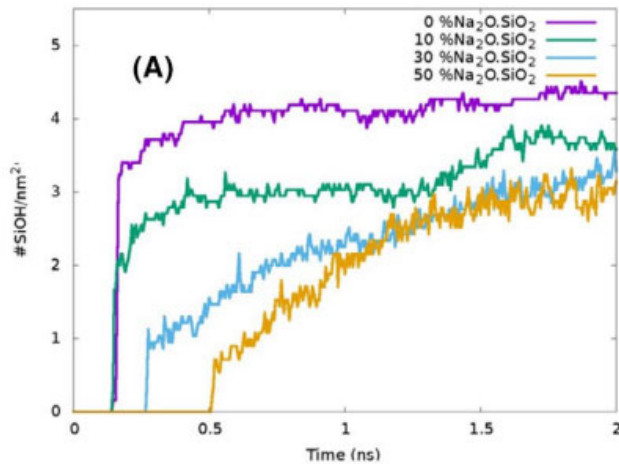


- Dissociable water potential obtained by force matching of AIMD results.
- Can describe reactions as well as physical properties of water
- Originally for water-silica system and recently added Na, Ca, Al to the potential sets
- It has advantage of speed (~10x faster than ReaxFF)

# Sodium silicate glass-water reactions



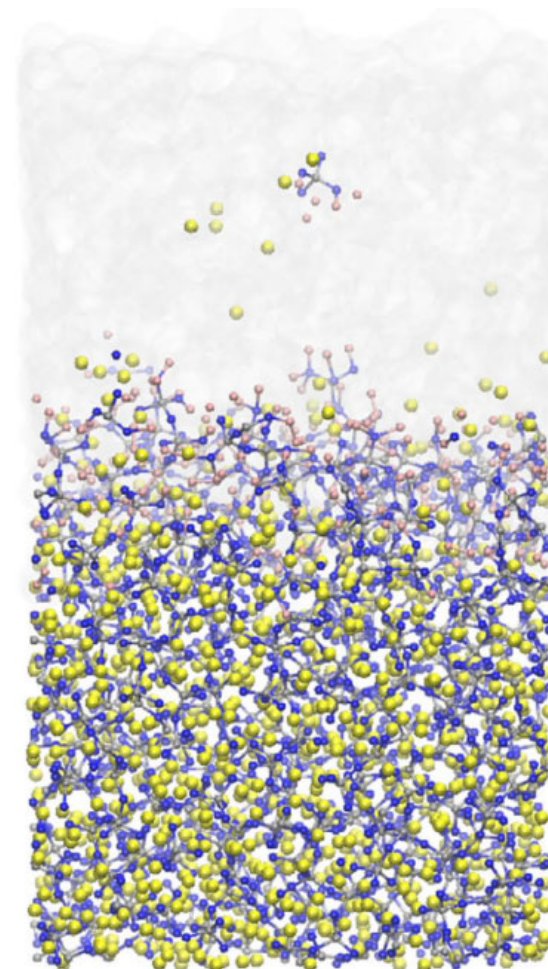
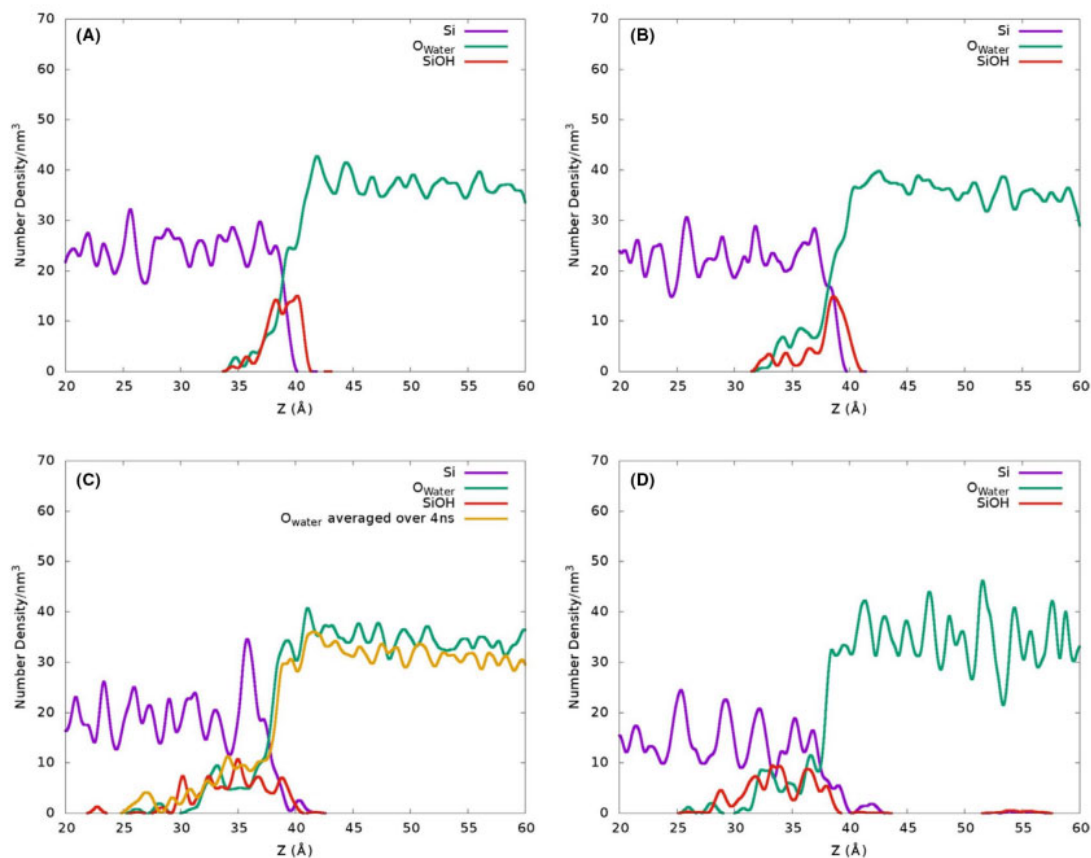
30Na<sub>2</sub>O-70SiO<sub>2</sub>



- Silica and a series  $x\text{Na}_2\text{O}-(100-x)\text{SiO}_2$  ( $x=10-50$ ) glasses were modeled using the DCRP potential
- Glass composition has a strong effect on initial glass-water interaction, or wetting of the glass surface

Mahadevan and Du, J. Am. Ceram. Soc. 103(2020)3676

# Na silicate glass-water reactions: glass composition effect



30Na<sub>2</sub>O-70SiO<sub>2</sub> glass-water reaction, 300K, DCRP potential

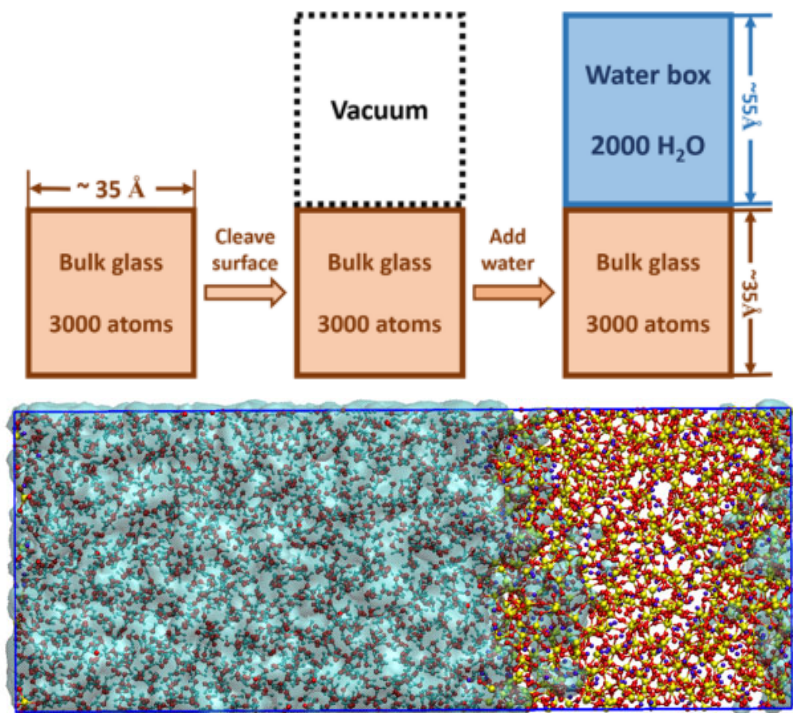
Mahadevan and Du, J. Am. Ceram. Soc. 103(2020)3676

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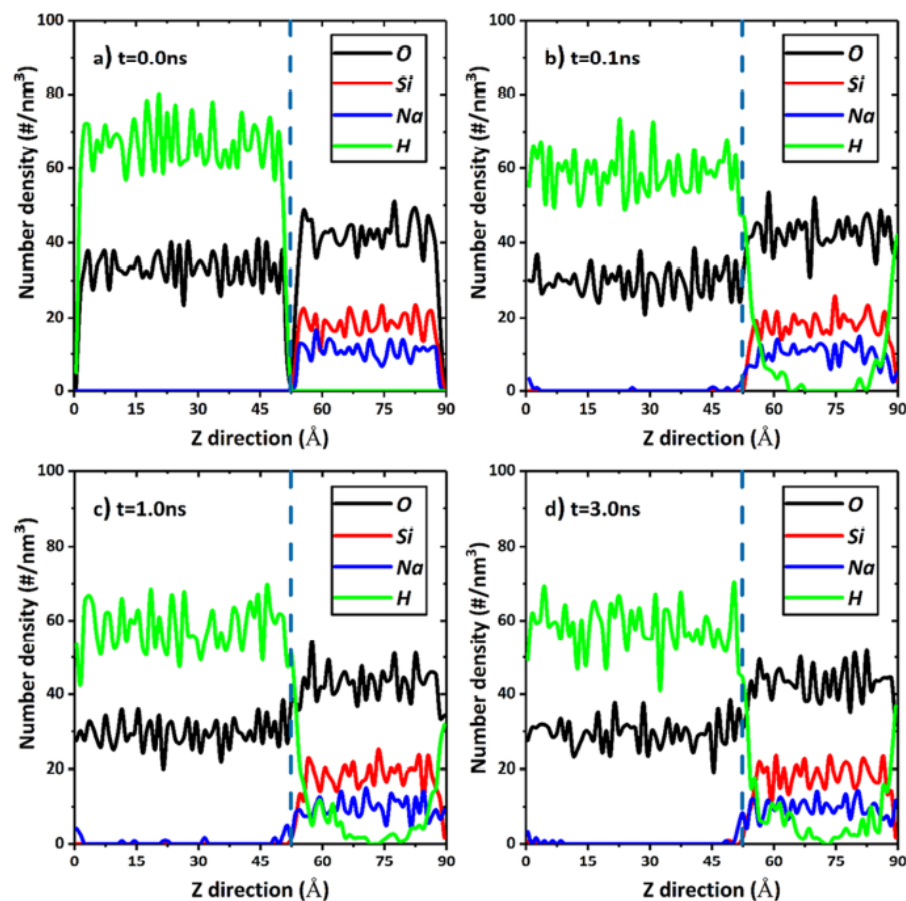
**UNT**  
UNIVERSITY  
OF NORTH TEXAS  
EST. 1890

# Sodium silicate glass - water reactions from reactive MD simulations



- ReaxFF based MD simulations up to 3 ns
- 77SiO<sub>2</sub>-23Na<sub>2</sub>O glass
- Four temperatures studied

Hahn et al. J. Phys. Chem. 122(2018)19613



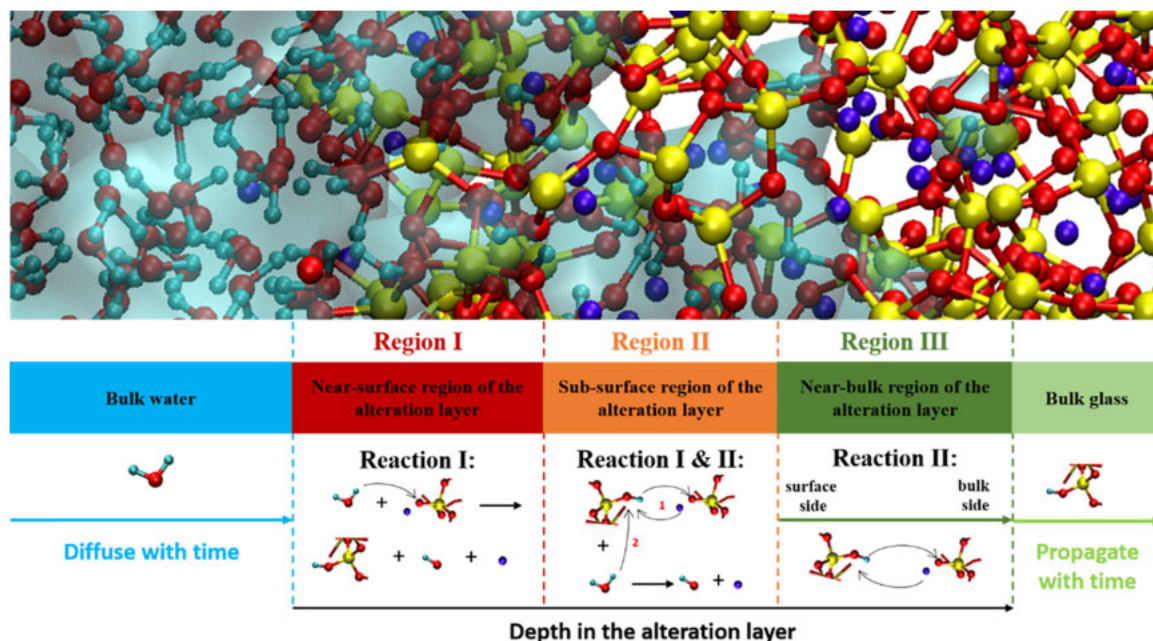
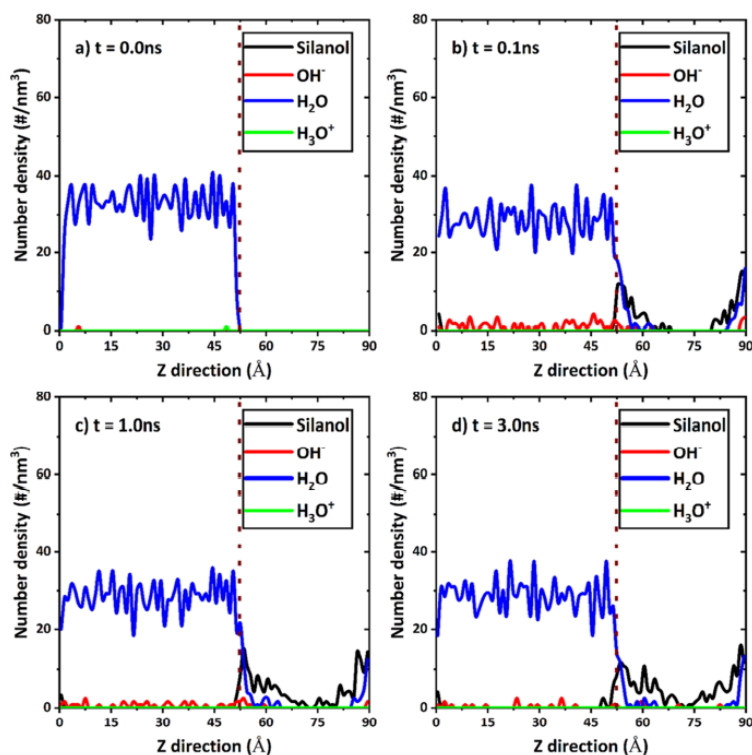
Deng et al. J. Phys. Chem. 123(2019)21538

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# Sodium silicate glass-water reactions: mechanisms

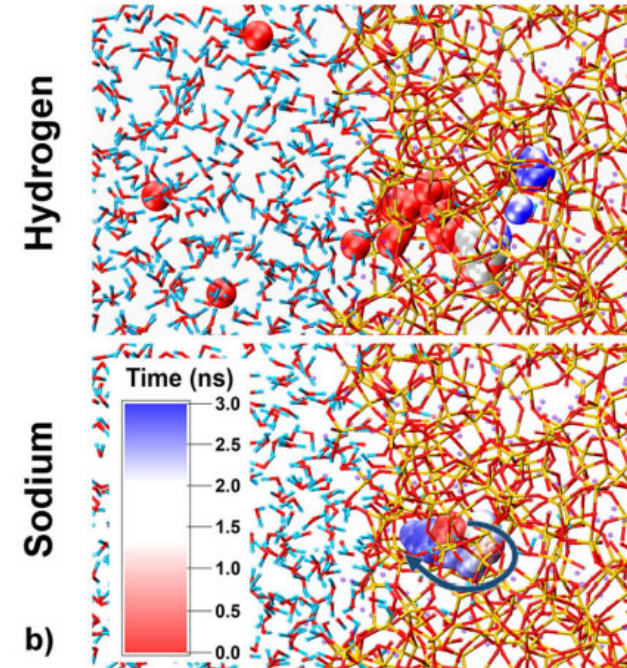
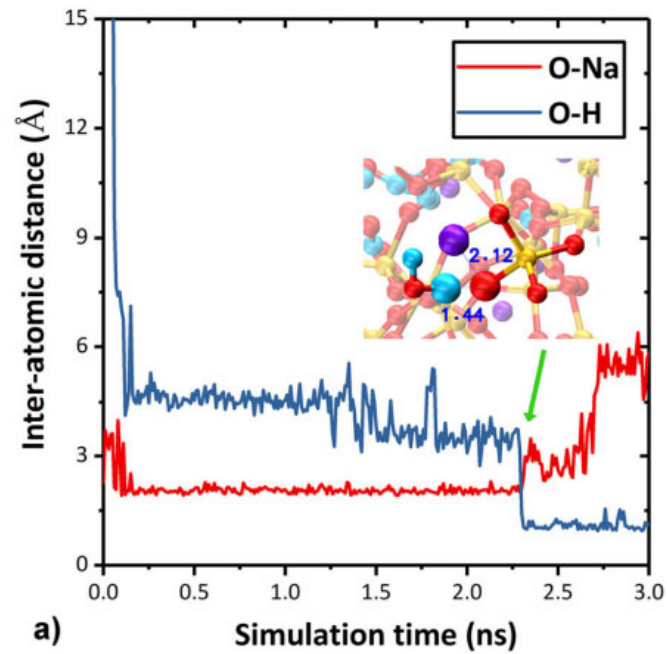
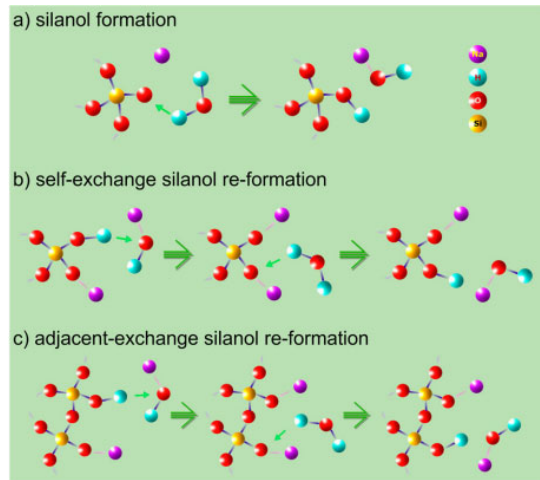
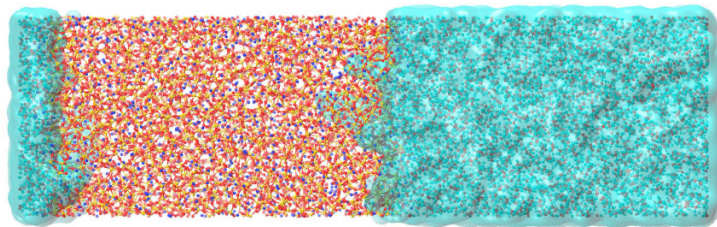


- ReaxFF based MD simulations up to 3 ns
- $77\text{SiO}_2\text{-}22\text{Na}_2\text{O}$  glass

- Water react with the glass surface (NBO) through hydration reactions:  $\text{Si-ONa} + \text{H}_2\text{O} \rightarrow \text{Si-OH} + \text{Na}^+ + \text{OH}^-$
- Further reaction mainly through proton transfer deeper into the glass (possible ion-exchange).

Deng et al. J. Phys. Chem. 123(2019)21538

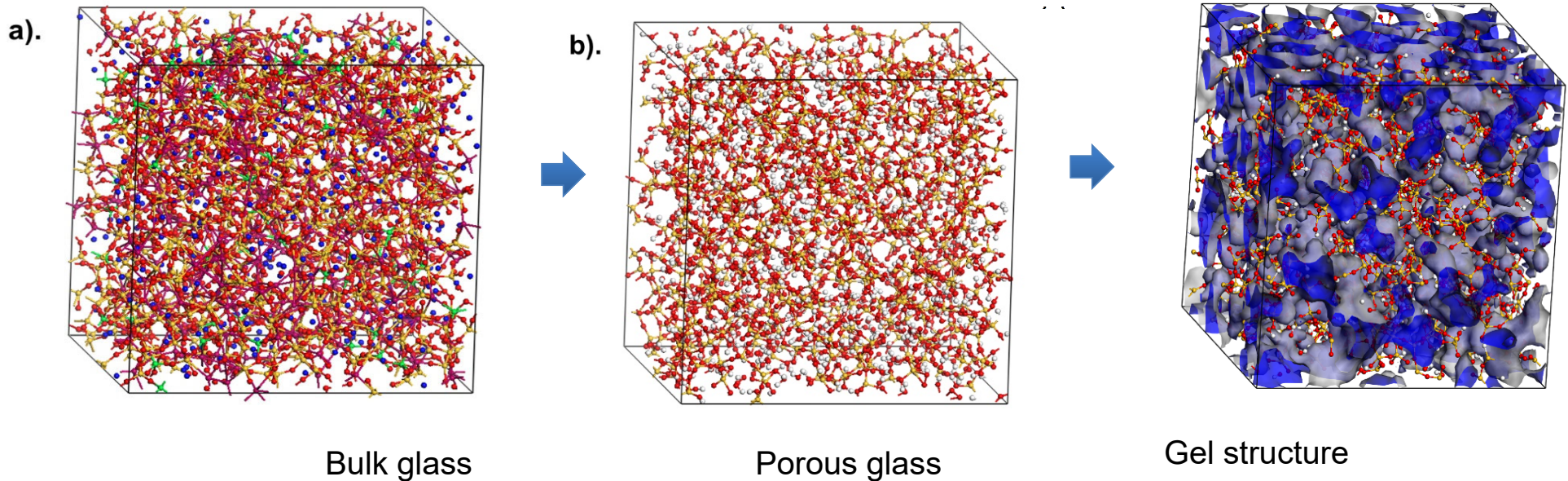
# Ion-exchange reactions in Na Silicate glasses



- ReaxFF based MD simulations with 0.1fs time step
- 77SiO<sub>2</sub>-23Na<sub>2</sub>O glass
- 300K and 450K simulations
- Direct observation of H<sup>+</sup>/Na<sup>+</sup> ion-exchange process

Deng et al. npj Mater. Degrad. 1(2021)15

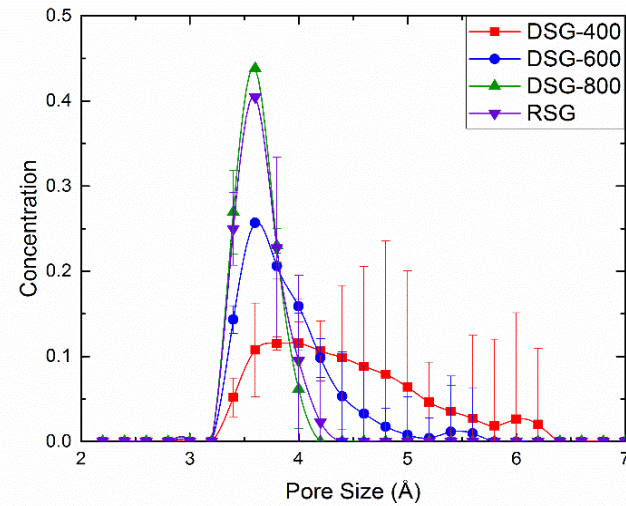
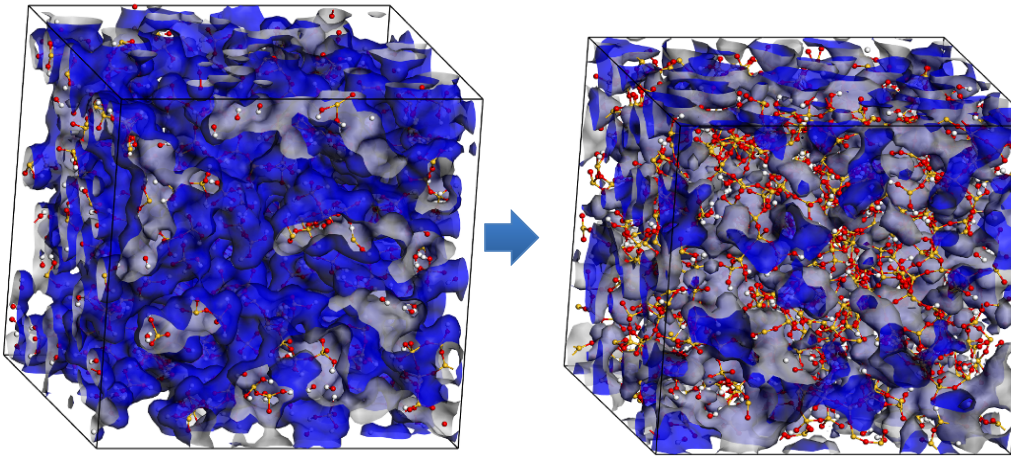
# Silica gel structure generation from bulk glass structure



- Two ways to generate gel layer structures: from preferential dissolution of ISG bulk glass structure
- From vacancy defect formation from dense silica
- Effect of formation method on atomic and microstructures evaluated. Water diffusion in the two structures examined.

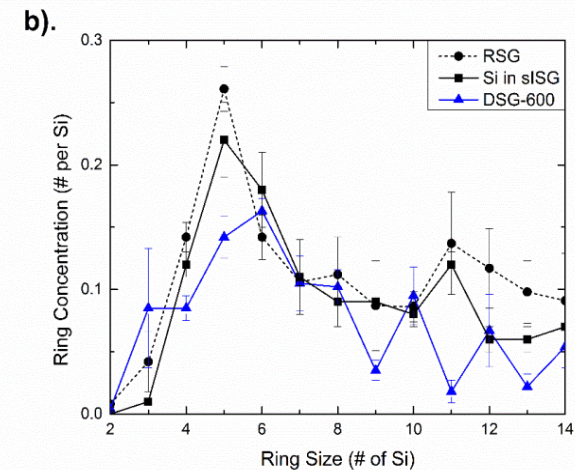
*Rimsza and Du, NPJ Mater. Degrad. 2018*

# Silica gel structure generation MD from dense silica



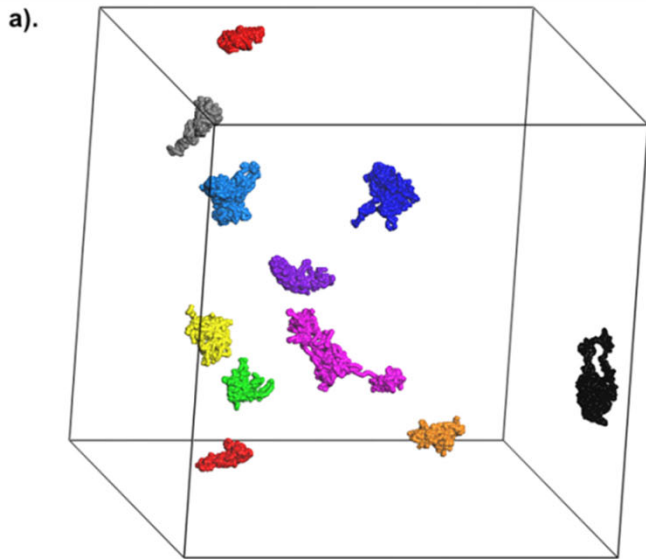
- Gel structure from dense silica with different porosity with ReaxFF based MD
- Si<sup>4+</sup> were randomly removed and replaced by H<sup>+</sup>, e.g. hydrogarnet defect formation.
- DSG-600 and RSG (from ISG) show similar ring and pore size distributions

Rimsza and Du, NPJ Mater. Degrad. 2018

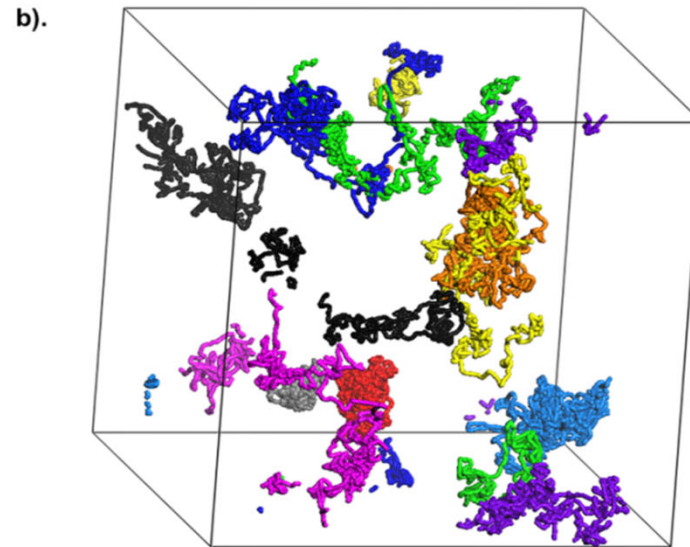


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# Water diffusions in porous gel structures

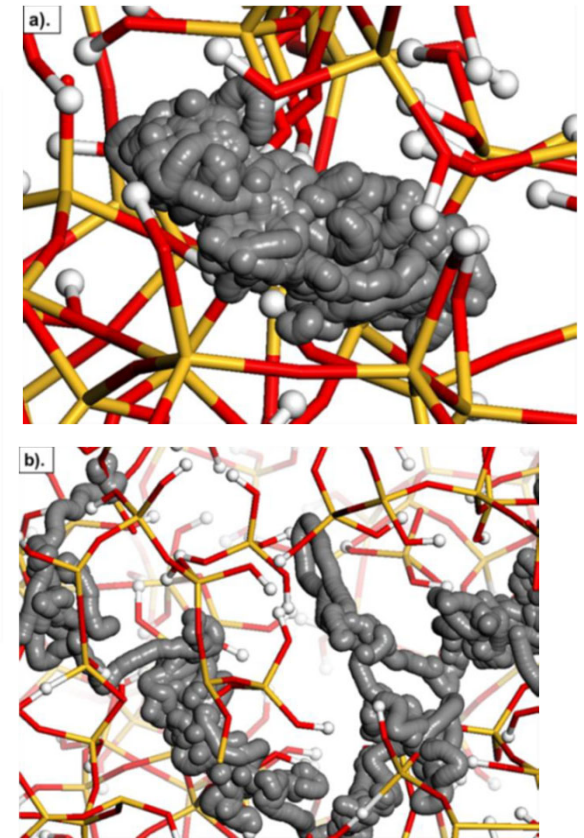


RSG (from ISG)



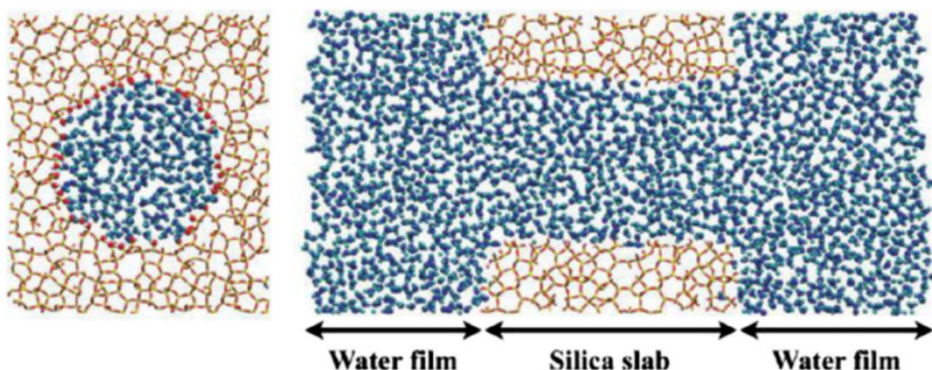
DSG-600 (from bulk silica)

- Similar pore size distribution and porosity but different diffusion behaviors. Remnant gel structures need further corrosion for water transport.



Rimsza and Du, NPJ Mater. Degrad. 2018

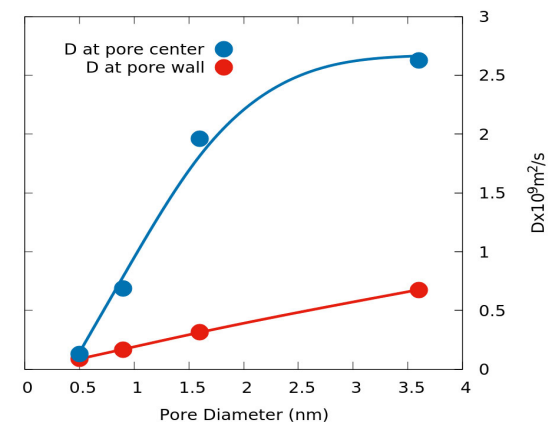
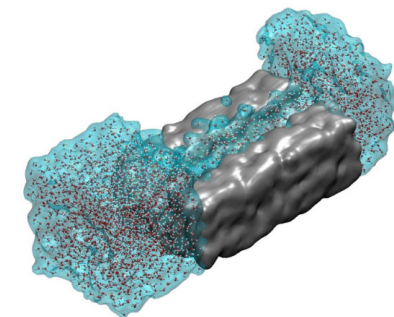
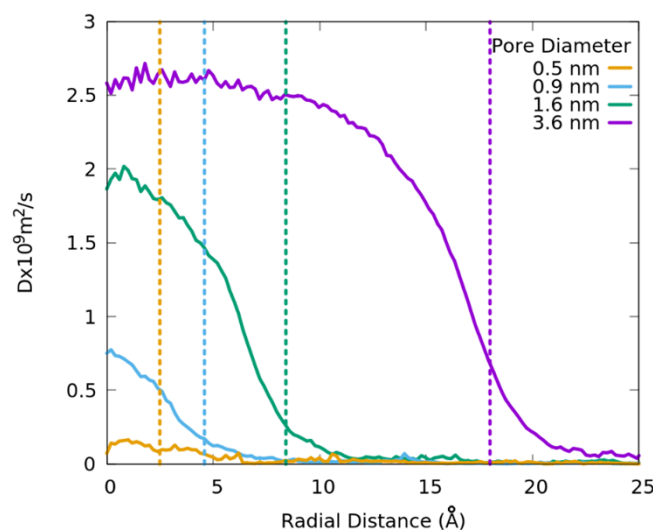
# Diffusivity of water in confined geometry



I. Bourg, JPCC 116 (2012) 11556

- Pore size determines the diffusivity at the center – larger pores attain unrestricted water diffusion at the pore center
- Diffusion in the hydrogen bonded network at the wall is always lower (under all confinements)

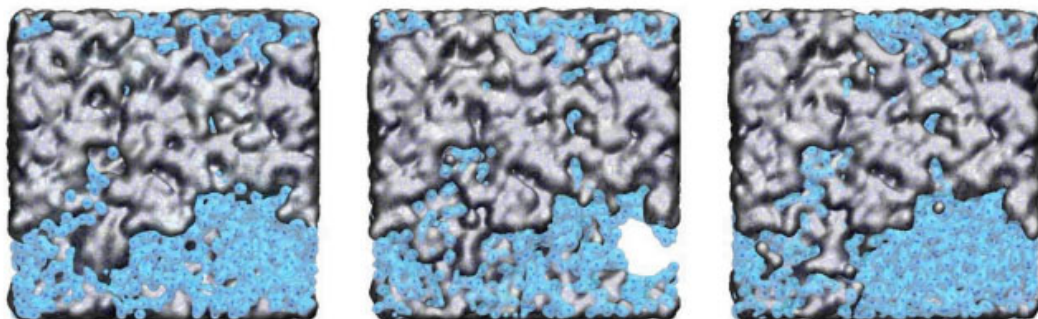
Colin et al, J Phys Chem C 2018  
Gin et. al Nature Comm. 2019



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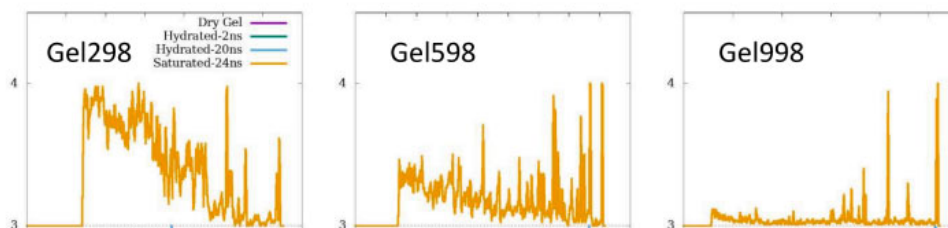
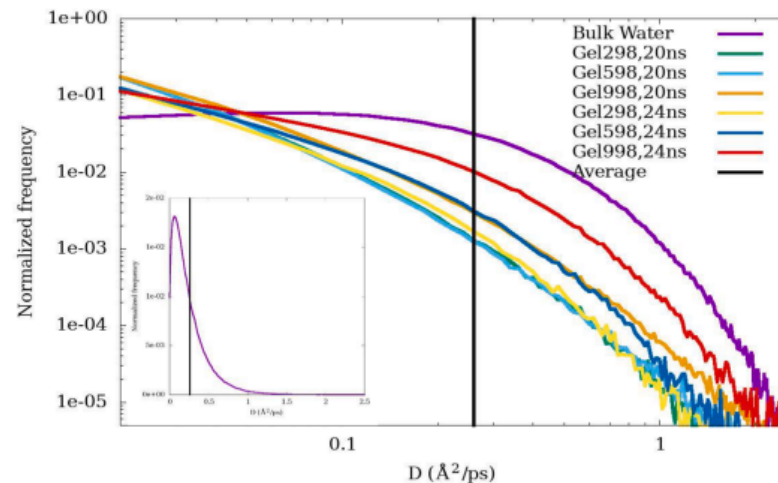
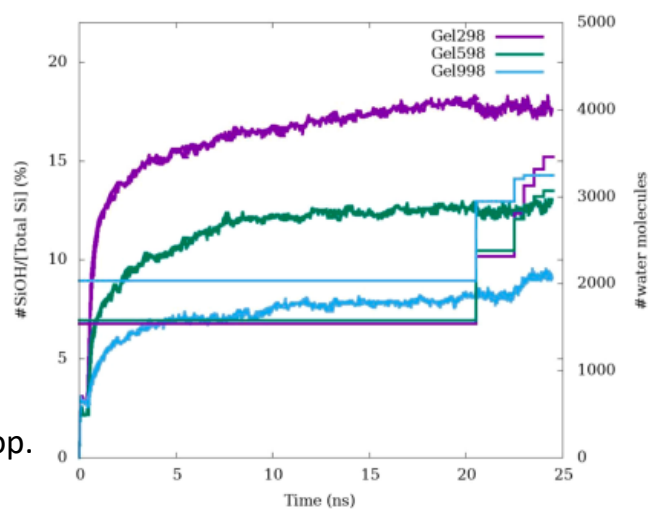
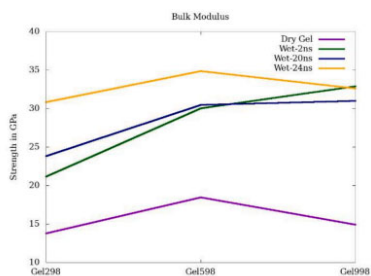
# Properties of CaO-Al<sub>2</sub>O<sub>3</sub>-SiO<sub>2</sub> porous gel structures



(a)

(b)

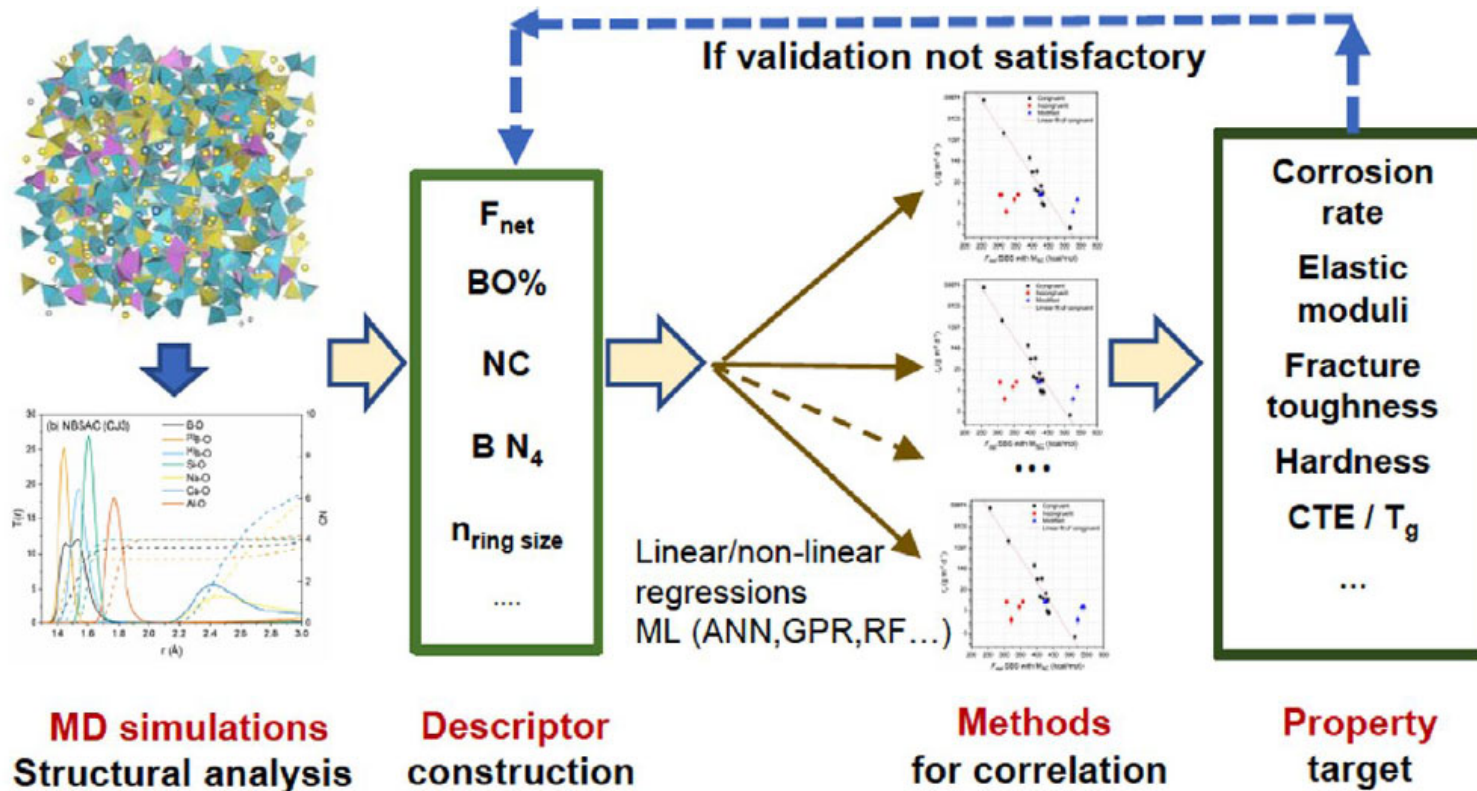
(c)



Mahadevan, Du, JNCS 621(2023)122604

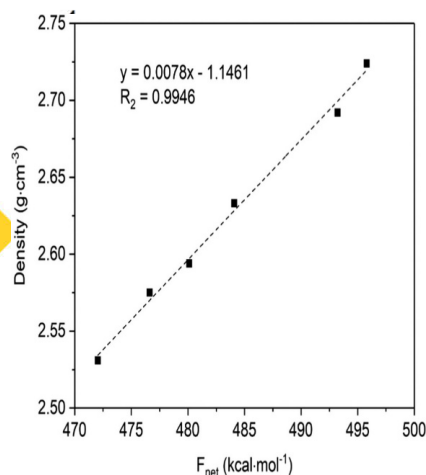
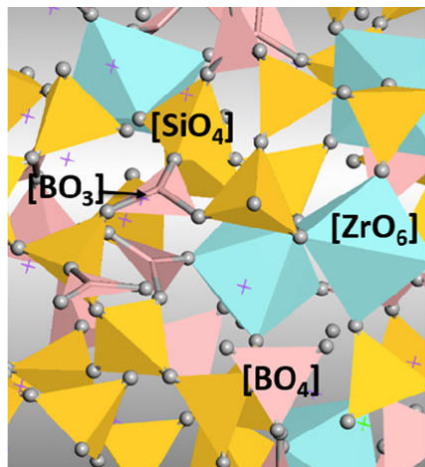
- DCRP reactive potential
- Up to 24 ns simulations
- Diffusion, mechanical prop.

# QSPR analysis of glass corrosion rate based on MD

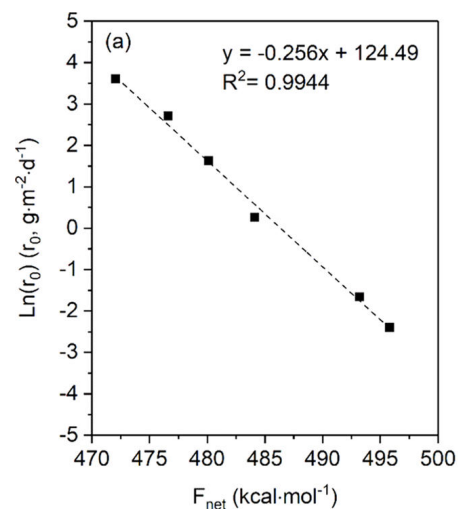




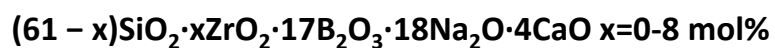
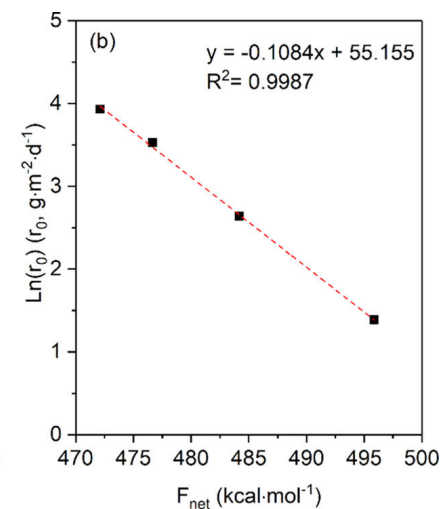
## MD based QSPR analysis of properties of ISG+ZrO<sub>2</sub> glass



Density



Initial dissolution rate r<sub>0</sub>

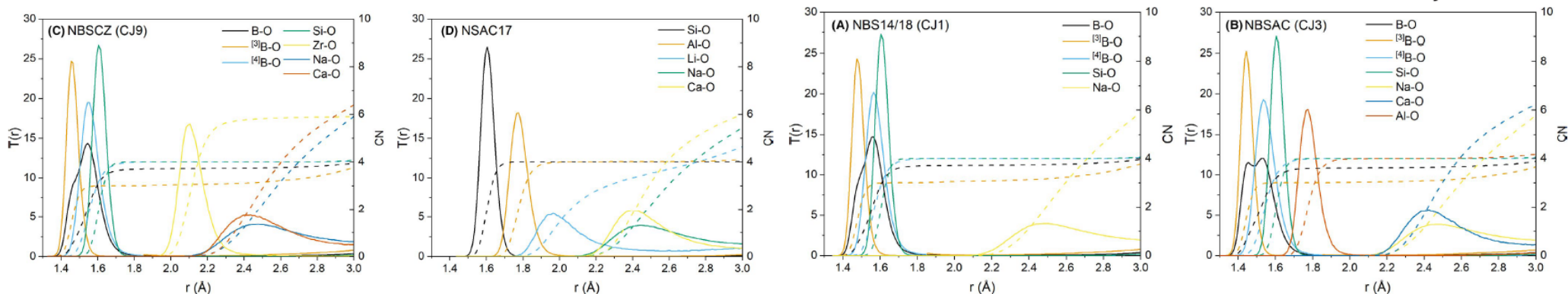


Two sets of experimental measurements for forward rate (r<sub>0</sub>) available:

- Cailleteau et al. 90 °C in buffered solution (pH=6.9) without agitation
- Bergeron et al. 90 °C single pass flow through measurement
- Flow through measurements gave corrosion rate an order of magnitude higher for high ZrO<sub>2</sub> composition
- QSPR analysis provide excellent correlation of both sets of data: consistency of experimental data set

*Lu, Deng, Gin, Du, J. Phys. Chem. B 123 (2019) 1412*

# Structures of aluminosilicate and borosilicate glasses from MD

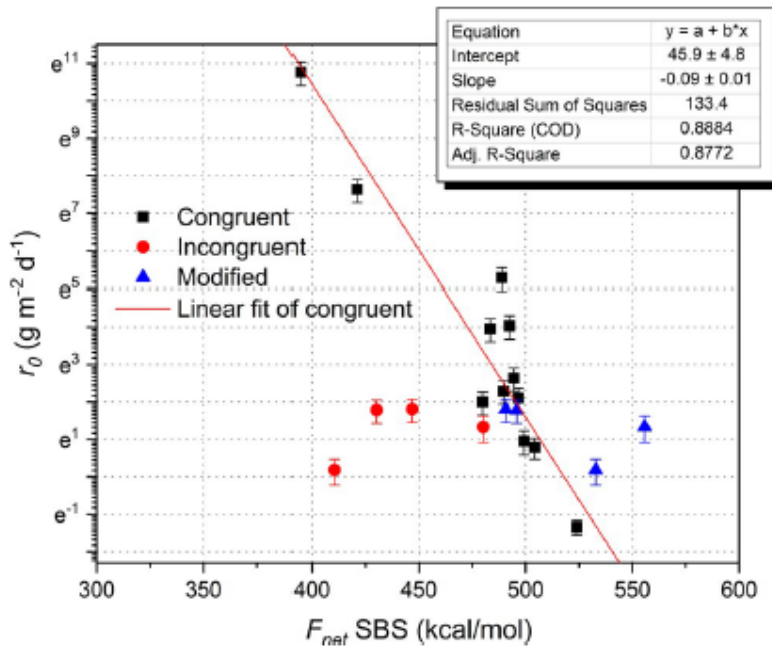


Glass	N <sub>4</sub> (%)				Oxygen speciation (%)			Ring size	
	YDBX <sup>63,64</sup>	Modified Bernstein <sup>65</sup>	MD	Exp. <sup>18</sup>	NBO	BO	TBO	Average size	>6, %
NBS14/18	73.5	65.8	70.2 ± 0.3	66	2.6 ± 0.1	96.4 ± 0.2	1.0 ± 0.1	7.28 ± 0.02	64.7 ± 0.6
NBSA	55.0	54.6	57.9 ± 0.3	48	1.8 ± 0.0	96.0 ± 0.1	2.3 ± 0.1	7.23 ± 0.02	63.9 ± 0.8
NBSAC	61.5	54.5	59.3 ± 0.5	53	5.9 ± 0.2	93.2 ± 0.4	0.9 ± 0.2	7.54 ± 0.04	66.7 ± 1.4
NBSACZ	62.3	52.9	61.3 ± 1.1	48	4.9 ± 0.2	93.3 ± 0.2	1.8 ± 0.1	7.40 ± 0.04	64.7 ± 0.6
NBSAZ	44.1	53.0	52.6 ± 0.8	41	1.6 ± 0.1	95.6 ± 0.3	2.8 ± 0.2	7.21 ± 0.04	63.6 ± 0.5
NBSC	73.5	69.3	70.6 ± 0.7	66	8.1 ± 0.1	91.7 ± 0.1	0.3 ± 0.1	7.63 ± 0.01	67.2 ± 0.5
NBSCZ	73.5	60.7	71.1 ± 1.0	63	6.5 ± 0.2	92.7 ± 0.3	0.8 ± 0.1	7.43 ± 0.05	65.0 ± 1.1
NBS12/28	41.8	56.1	42.6 ± 0.5	43	1.0 ± 0.1	97.8 ± 0.2	1.2 ± 0.1	7.97 ± 0.05	74.8 ± 0.8

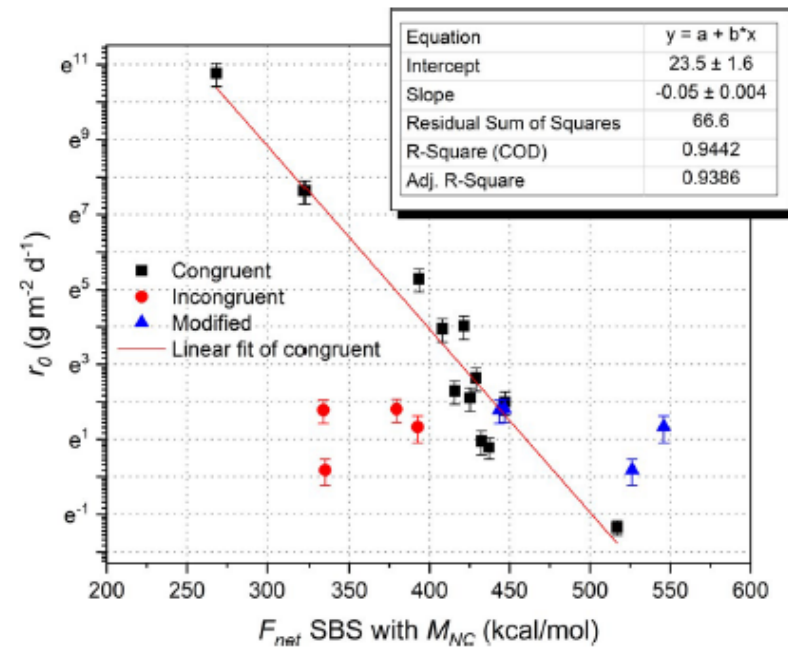
SumGlass 2023, Nimes France, du@unt.edu

# Correlation of initial dissolution rate with $F_{net}$

**F<sub>net</sub>: regular definition**  
**R<sup>2</sup>=88.8%**



**F<sub>net</sub>: modified definition**  
**R<sup>2</sup>=94.4%**



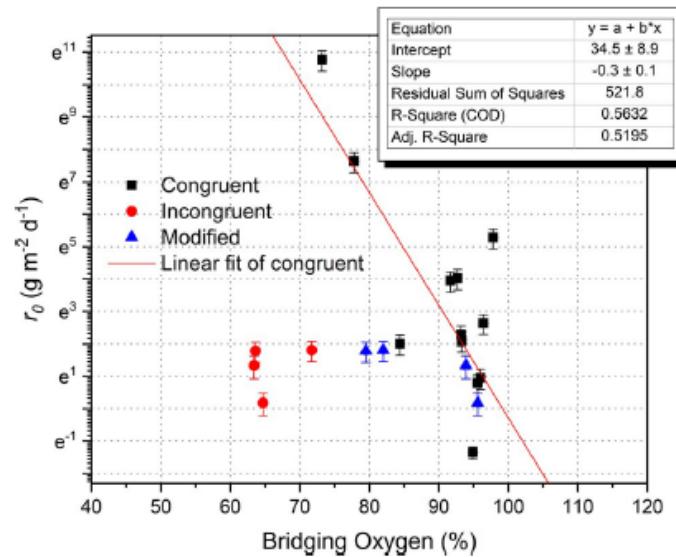
$$F_{net} = \frac{1}{N} \sum_X^{cations} n_X \cdot CN_{XO} \cdot SBS_{XO} \cdot m_X$$

Modifying the descriptor by introducing network connectivity improves the fitting.

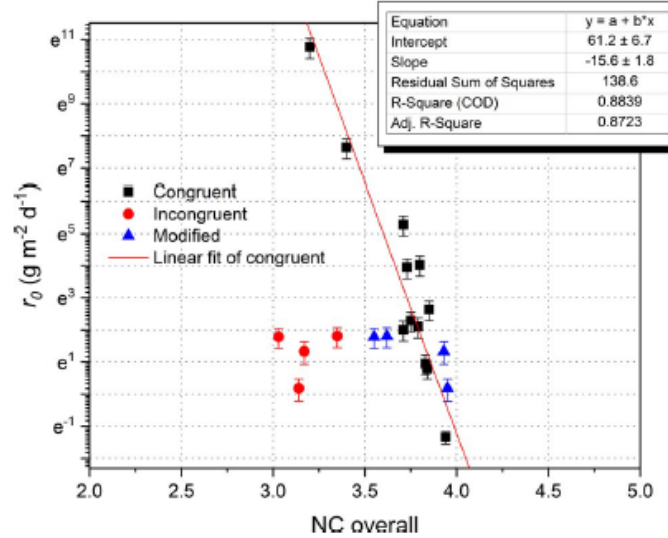
Du et al. J. Am. Ceram. Soc. 104(2021)4445

# Using structural features as descripts

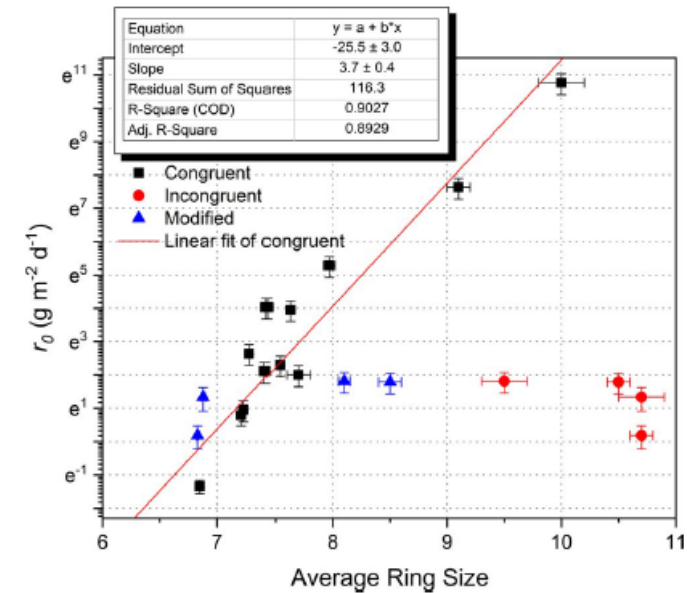
**BO percentage**  
 $R^2=56.3\%$



**Average network connectivity**  
 $R^2=88.4\%$



**Average ring size**  
 $R^2=90.3\%$

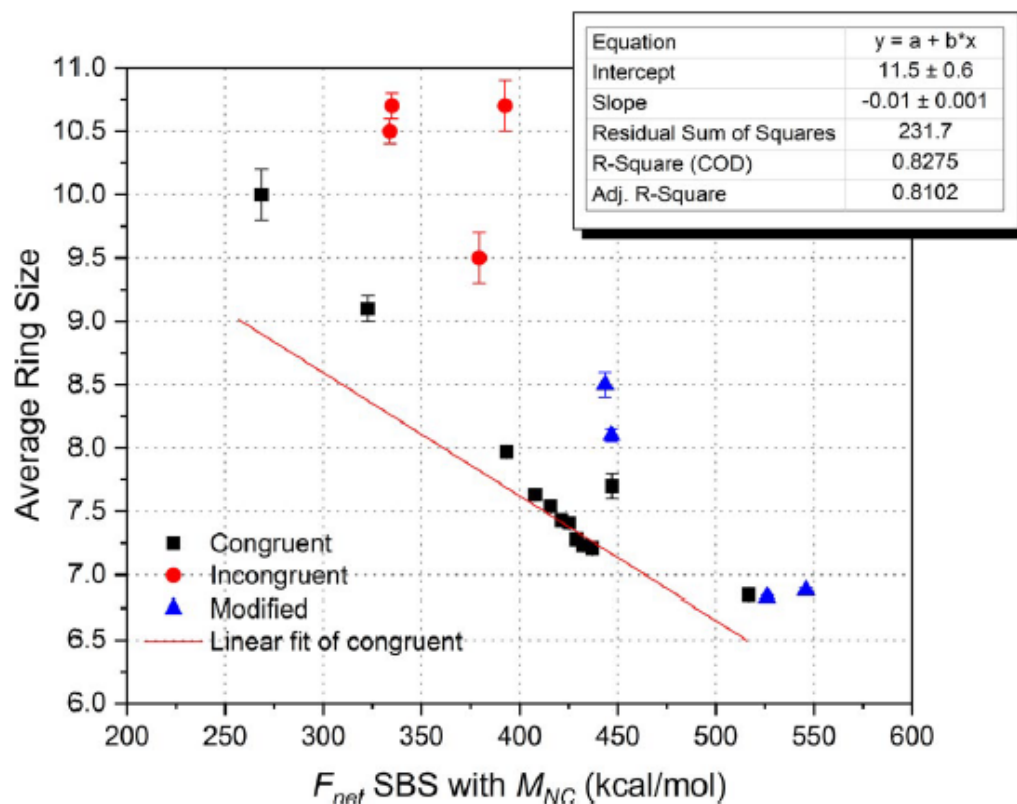
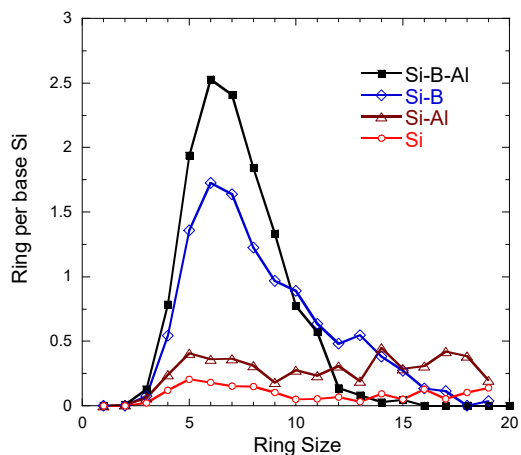
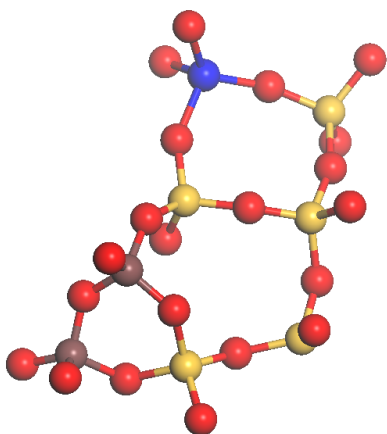


**FIGURE 6** Correlation between initial dissolution rate  $r_0$  ( $\text{g m}^{-2} \text{day}^{-1}$ ) and percentage of bridging oxygen (BO%)

**FIGURE 7** Correlation between initial dissolution rate  $r_0$  ( $\text{g m}^{-2} \text{day}^{-1}$ ) and overall network connectivity (NC), where Si, Al, B, and Zr are considered as network formers

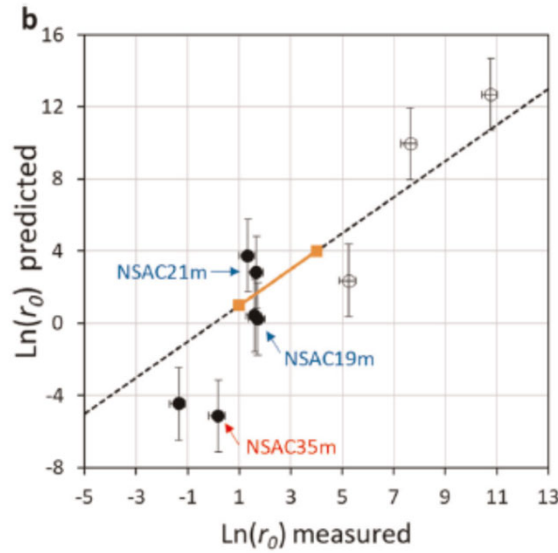
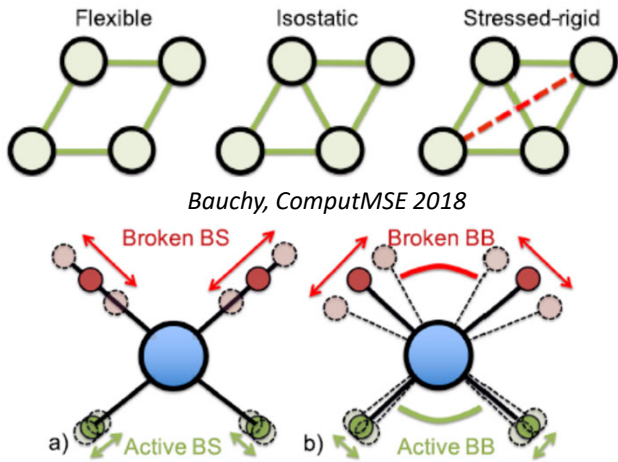
**FIGURE 8** Correlation between  $r_0$  ( $\text{g m}^{-2} \text{day}^{-1}$ ) and average ring size

# Correlation best the best descriptors



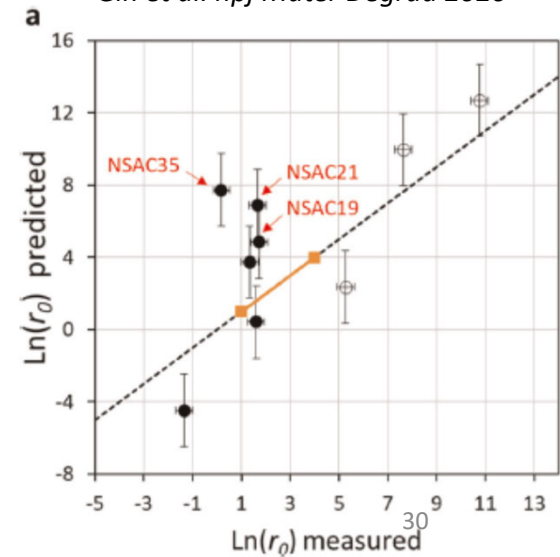
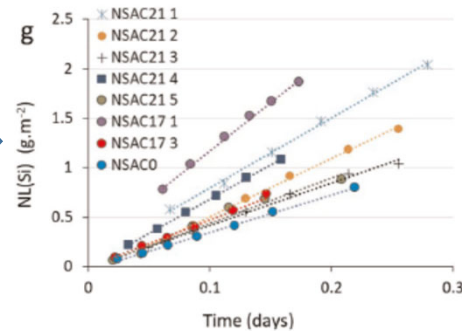
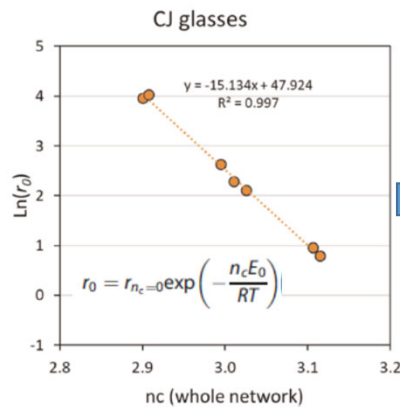
- Two best descriptors for initial dissolution rates are average ring size and  $F_{net}$  are linearly correlated
- Incongruent dissolution samples need to be modeled based on the modified composition
- Residual rate correlation possible by introducing descriptors with gel characteristics

# Correlation of borosilicate glass corrosion rate with TCT



- Topological constraint theory (TCT) is shown to be capable to correlate with initial corrosion rate ( $r_0$ ) for a wide range of borosilicate glasses
- Exceptions found in a few aluminosilicate glasses that have preferential leaching
- Correction of the composition can improve the correlation

	BS	BB
Si	4	5
B <sup>III</sup>	3	3
B <sup>IV</sup>	4	0
Al	4	5
Na	1	0
Ca	2	0
BO	0	1
NBO	0	0



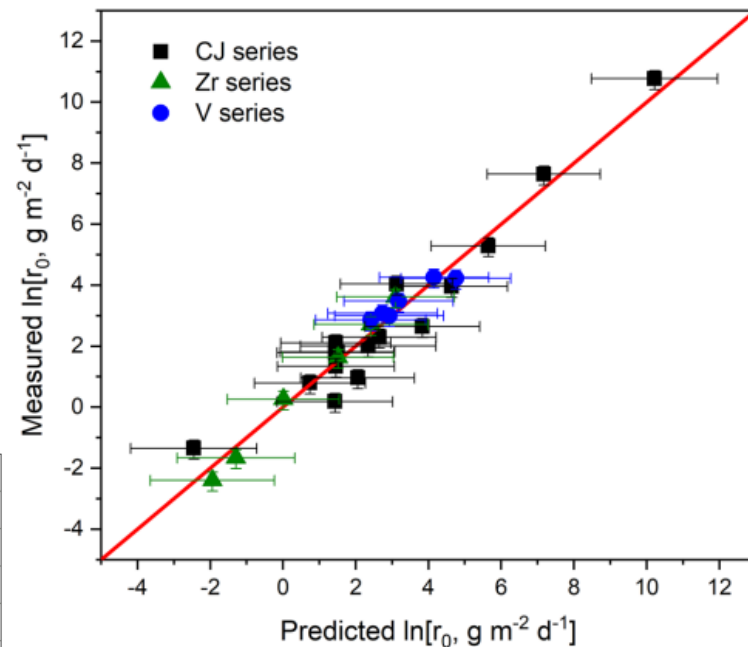
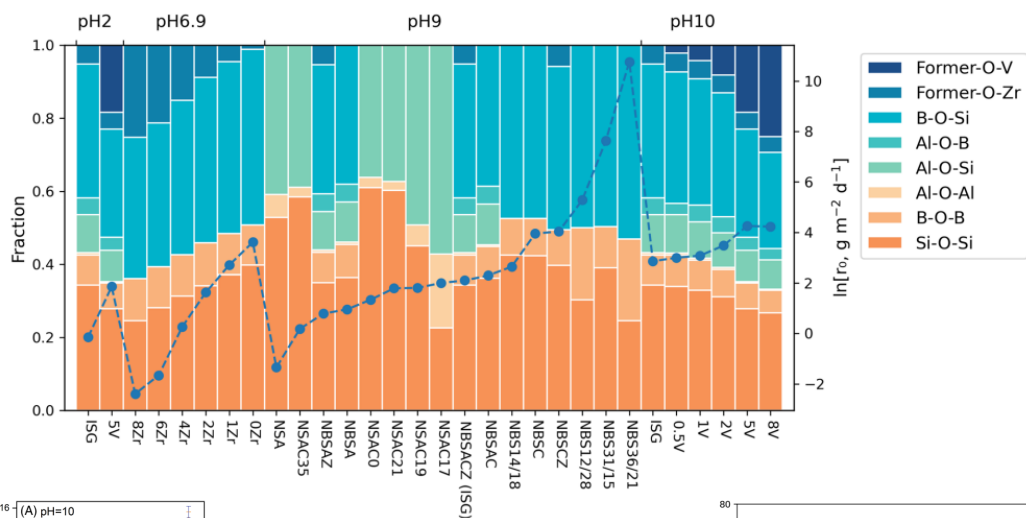
Gin et al. npj Mater Degrad 2020

SumGlass 2023, Nimes France, du@unt.edu



EST. 1890

# Predict dissolution rate from structure features from MD simulations



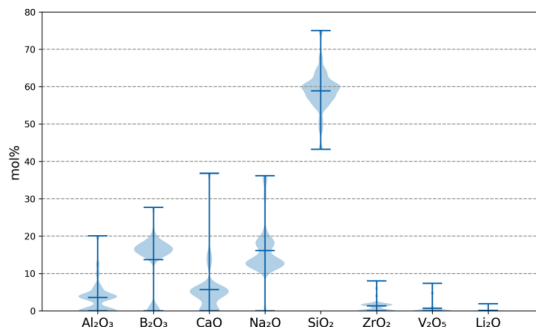
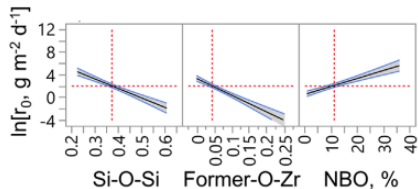
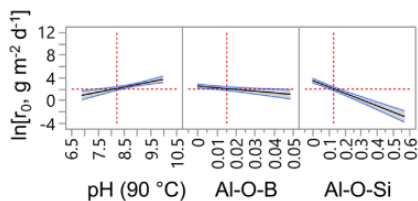
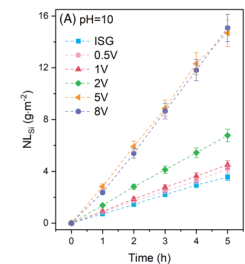
**Predicting initial dissolution rates using structural features from molecular dynamics simulations**

Xiaonan Lu<sup>1</sup> | Lu Deng<sup>2</sup> | Stéphane Gin<sup>3</sup> | Benjamin Parruzot<sup>1</sup> | Joelle T. Reiser<sup>1</sup> | Joseph V. Ryan<sup>1</sup> | John D. Vienna<sup>1</sup> | Jincheng Du<sup>2</sup>

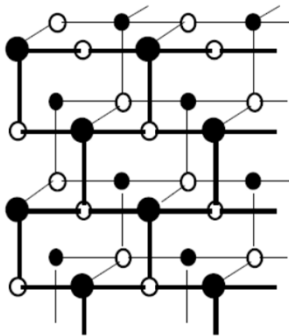
Lu et al. JACeS 106(2022)1025

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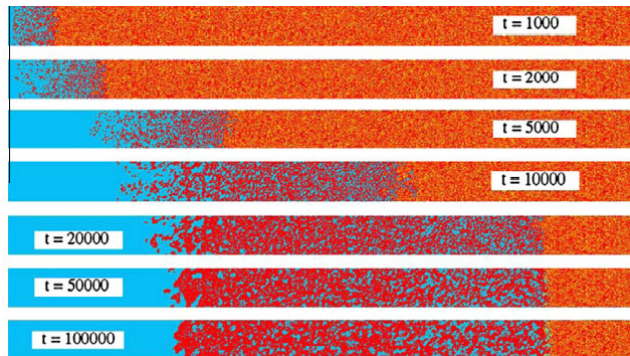
SumGlass 2023, Nimes France, du@unt.edu



# Monte Carlos simulations of glass corrosion



MC models rely on regular lattices to approximate glass structure

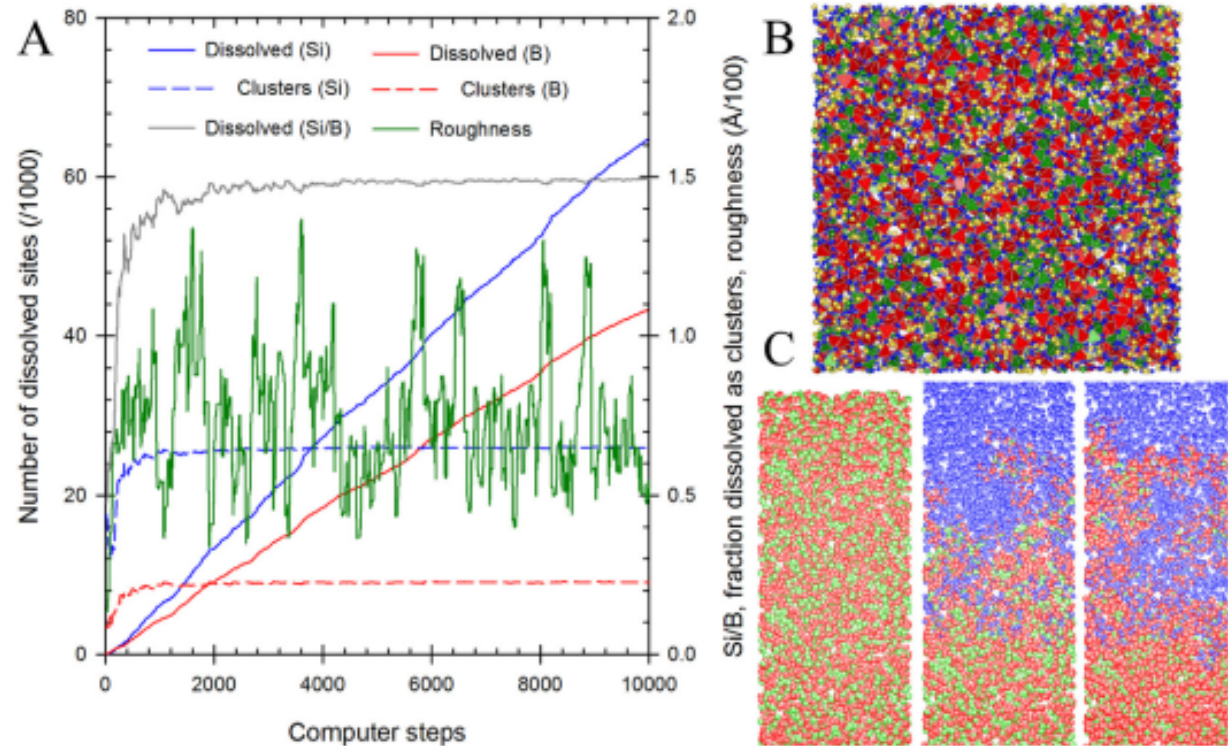


MC simulations of leaching of borosilicate glass



Devreux et al., JNCS 343(2004)13

MC simulation based on structure models from MD



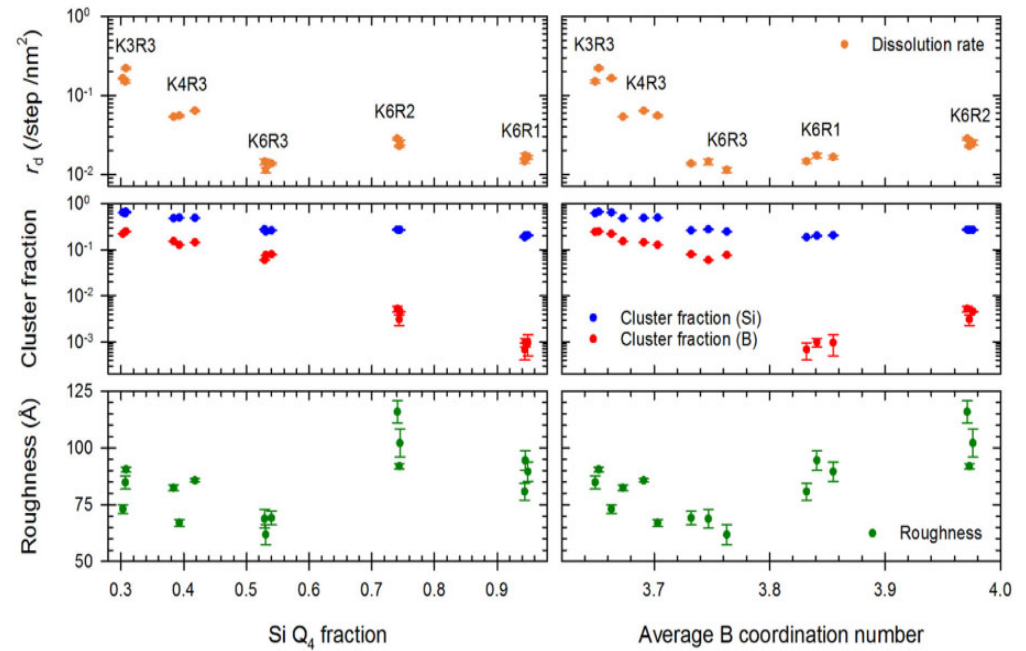
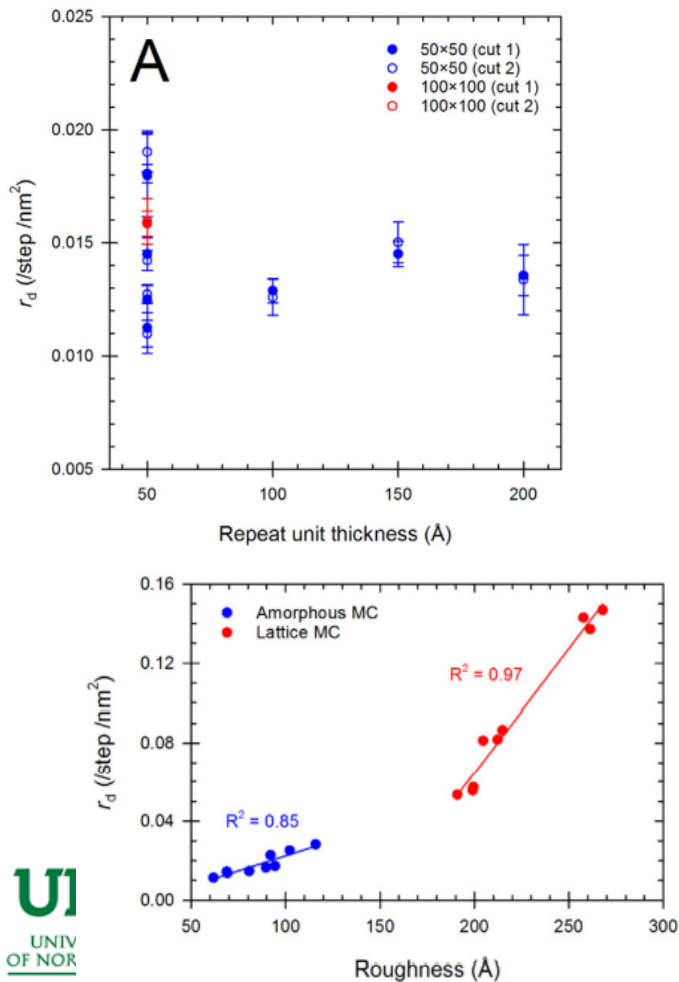
42.9 SiO<sub>2</sub>-14.3 B<sub>2</sub>O<sub>3</sub>-42.9 Na<sub>2</sub>O

Keresit & Du, *J. Non-Cryst. Solids*, 522(2019)119601

SumGlass 2023, Nimes France, du@unt.edu



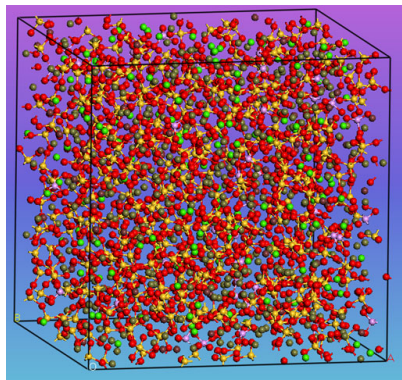
# Monte Carlos simulations of sodium borosilicate glass corrosion



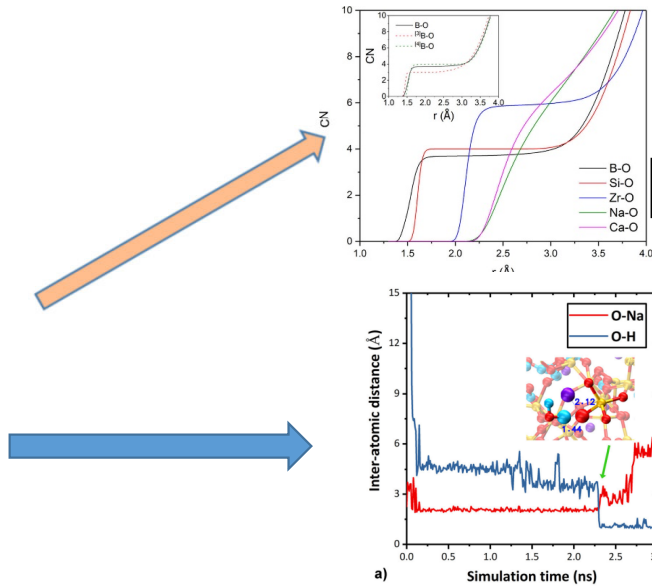
- MC based on glass structure generated from MD
- Effect of repeating unit thickness on dissolution rate investigated
- Dissolution rate and surface roughness studied as a function of glass composition
- Surface roughness a lot lower than regular lattice models

Keresit & Du, *J. Non-Cryst. Solids*, 522(2019)119601

# Understand of Glass Corrosion with MD based Simulations

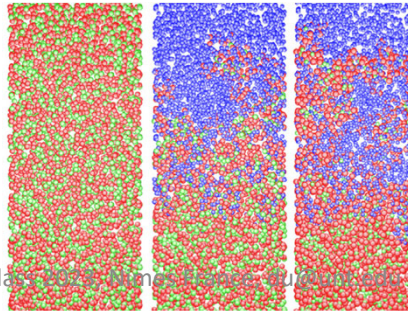


Glass structure from MD simulations & characterizations



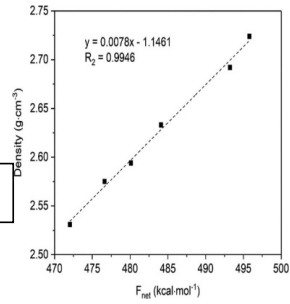
Reaction mechanism, interfacial structure/evolution

MC simulations of glass corrosion



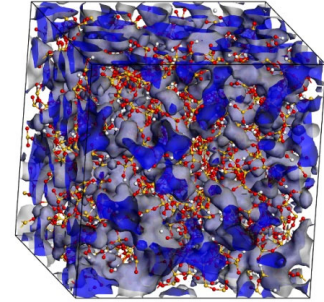
SumGlas 2022, SumGlas, https://doi.org/10.26434/chemrxiv-2022-33333

QSPR analysis



Lu et al. npj Mater. Degrad 2019  
Du et al. J. Am Ceram. Soc 2021

Gel structure and transport



Rimsza and Du, JPCC 2018  
Deng et al, JPCC 2018  
Deng et al. npj Mater Degrad 2019

Kerisit, Du, JNCS 2019  
Kerisit, Mahadevan, Du, JNCS 2021

Glass dissolution mechanism & corrosion rate prediction

# Conclusions and outlook

- Atomistic simulations and particularly classical MD simulations are highly valuable tools to understand nuclear waste glass structures and glass-water interactions.
- Development of interatomic potentials (reactive and non-reactive) are needed to enable some of these simulations.
- Complex nuclear waste glass structures, including redox effect and phase separation, can be studied as a function of glass composition.
- Interfacial structures of water/glasses are modeled to understand the corrosion gel structures. Diffusion and other properties can be investigated in the bulk, the gel and the interface.
- MD based QSPR approach valuable for corrosion rate and other property predictions
- Machine learning has been increasingly used with the MD data or other structure features from glasses.

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Jerry Frankel (Ohio State)

Seong Kim (Penn State)

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### Graduate students/postdocs:

Lu Deng, TS Mahadevan, Xiaonan Lu,  
Jessica Rimsza, Wei Sun, Wenqing Xie,  
Jayani Kalahe, Mengguo Ren

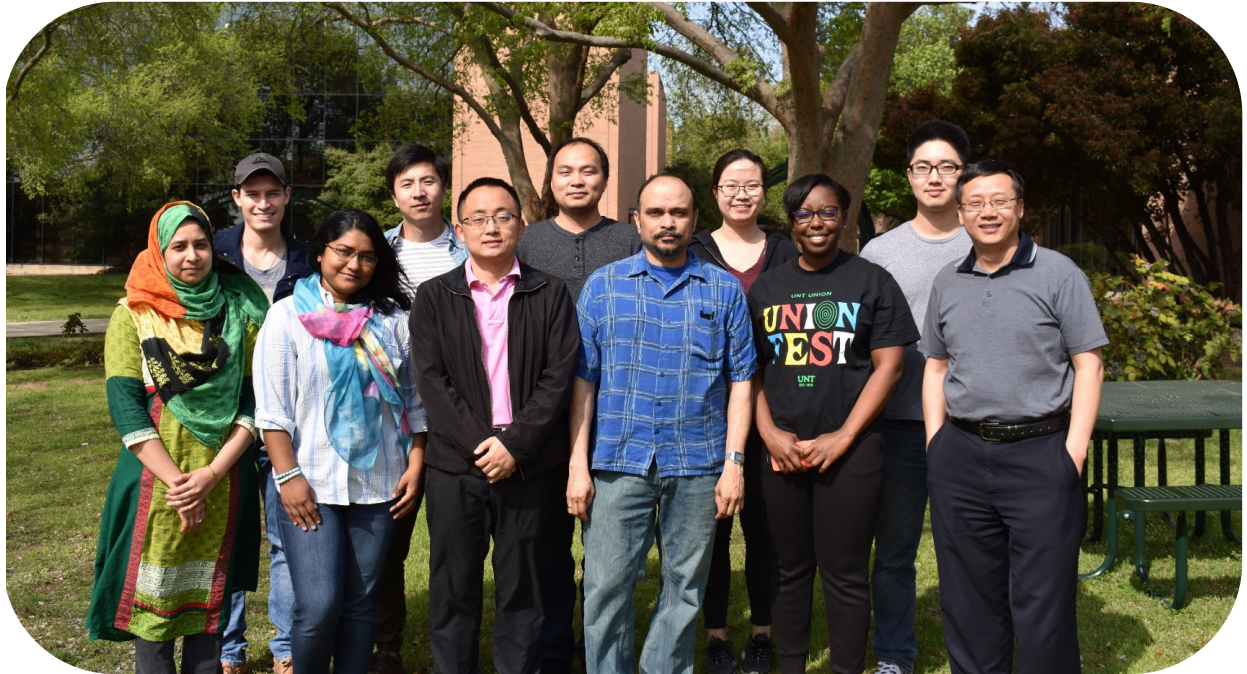
### Funding support:

DOE NEUP DOE EFRC Waste PD  
NSF DMR Ceramics, AGC, Corning Inc.

### Computer Time Support:

TACC, UNT Talon3, Cruntch3/4

## Functional Glasses and Materials Modeling Laboratory



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EST. 1890



**WASTE PD**  
*Performance and Design*



**NEUP**  
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*Thank you!*



TC27: Atomistic Simulation

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